

28.1 LOCATION OF STRUCTURE:

Alignment at existing km 358/1.

28.2 BOREHOLE DESCRIPTIONS:

- Location of Structure, Boreholes with RL shown in **FIGURE-1**.
- Subsurface Characteristic of Soil/Rock shown in **ANNEXURE-I**.
- Borelogs and sub soil profile shown in **ANNEXURE-II**.
- Calculations of Safe Bearing Capacities in **ANNEXURE-III**.
- Calculations of Probable Settlement in **ANNEXURE-IV**.
- Depth of water Table $\geq 16.00\text{m}$ below EGL.

Subsurface profile at the site

BOREHOLE No.	Depth (m)	Type of Soil/Rock	Soil/Rock Characteristics
BH-1	0.00 to 1.50	Sandy Silt	Loose
	1.50 to 3.00	Sandy Silt	Medium Dense
	3.00 to 12.00	Silty Sand	Medium Dense

28.3 CHEMICAL ANALYSIS OF SOIL:

BOREHOLE		CHEMICAL PROPERTIES					
No.	Depth (m)	pH	Carbonate	Chlorides %	Sulphate %	Nitrate %	Salinity %
BH-1	3.00	8.50	0.008	0.0016	NIL	0.0009	0.031

28.4 DIFFERENTIAL FREE SWELL INDEX (DFS)

Bore Hole No.	Depth (m)	DFS Index in %
BH-1	3.00	NIL

28.5 NET ALLOWABLE BEARING PRESSURE

Borehole No.	Depth from EGL (m)	Net Allowable Bearing Pressure (t/m^2)
BH-1	1.50	13.00
	3.00	18.00
	4.50	18.50
	6.00	19.50

28.6 CONCLUSIONS

- Subsurface Profiles indicates suitable Soil formation for foundations.

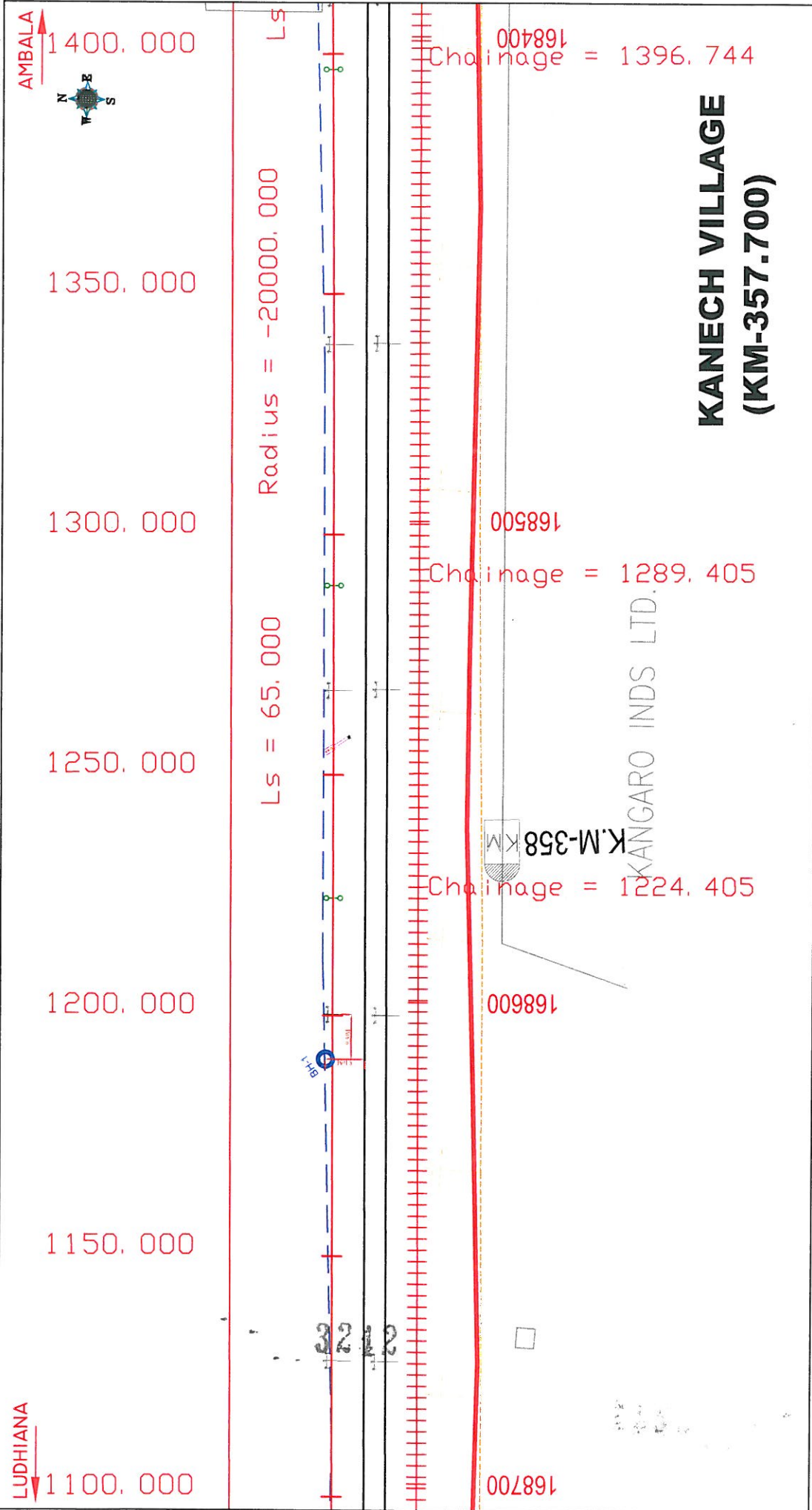
3240

28.7 RECOMMENDATIONS

(i)	<i>Type of foundation</i>	Open foundation
(ii)	<i>Depth of foundation below GL</i>	Below 3.00m from EGL

Note- The above recommendations are based on the field and laboratory tests conducted on the soil, and our experience in this regard. If the actual subsoil conditions during excavation for the foundation differ from the observations reported here, the design experts/consultants should be referred for suggestion, further investigations. However, the Depth and Type of foundation is to be decided by the structure designer depending upon the type of loading/structure and site conditions.

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ALL DIMENSIONS IN METER FIG.:-I LOCATION PLAN OF PROPOSED ALIGNMENT AT CH. 358/I	PROJECT :- LUDHIANA-AMBALA (DFCCIL)	DESIGN :- CONSULTING ENGINEERS GROUP LTD. E-12, Maji Colony, Malviya Nagar, Jaipur-17 Tel: +91-141-2520899, 2521899, 2520556 Fax: 2521348, E-Mail: ceeg@ceindia.com
	RL OF BH-I = 256.013	

ANNEXURE - I

Geotechnical Report

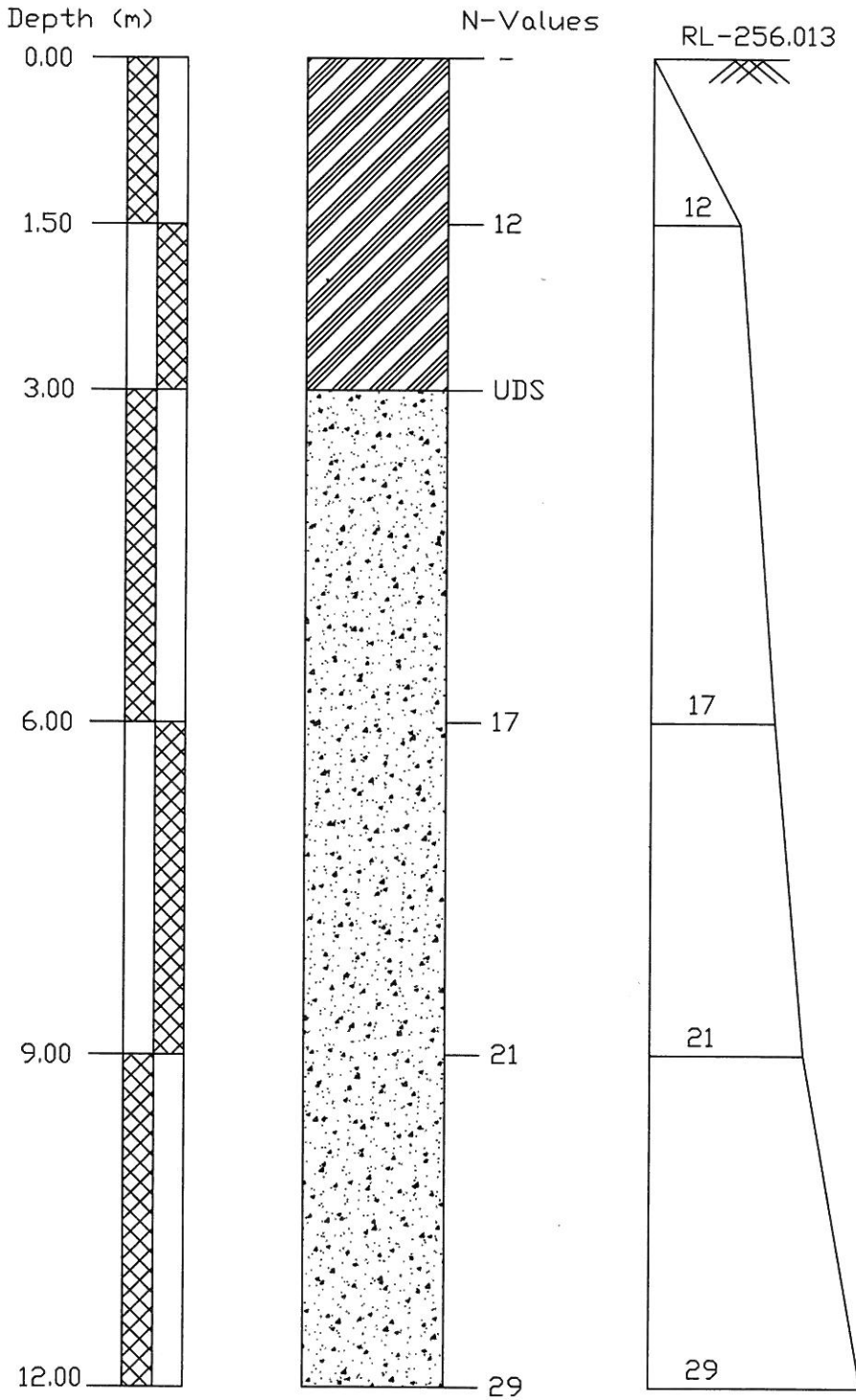
SOIL CHARACTERISTICS OF BORE HOLE AT BH-1 (LHS) OF ALIGNMENT AT CHAINAGE 358/1																				
Project : 3243	Chainage 358/1			Date of Testing		Location at		B.H. No.		Depth of Water Table		Termination Depth		Surface Elevation						
	Observed	Correction	Corrected	Soil		Clay	Silt	Fine	Medium	Coarse	Fine	Coarse	Gravel	Alterberg Limits %	B.D.	M.C	D.D.	Specific Gravity	Shear Strength	
Depth from GL (m)	N	C _n	N _n	Description (Soil Group)	2.57	65.72	13.26	14.29	2.37	1.15	0.64	0.00	22	NP	1.73	3.06	1.68	2.67	c kg/cm ²	φ degree
0.00	-	-	-	Sandy Silt	2.57	65.72	13.26	14.29	2.37	1.15	0.64	0.00	22	NP	1.73	3.06	1.68	2.67	-	-
1.50	12	1.45	17.40	Sandy Silt	3.18	50.13	46.45	0.24	0.00	0.00	0.00	21	NP	-	-	-	-	-	-	-
3.00	UDS	-	-	Silty Sand	1.75	7.39	85.02	3.27	1.90	0.67	0.00	28	NP	1.73	3.06	1.68	2.67	0.00	26.00	-
6.00	17	0.99	16.83	Silty Sand	3.38	12.06	83.41	1.10	0.05	0.00	0.00	29	NP	-	-	-	-	-	-	-
9.00	21	0.85	17.85	Silty Sand	2.64	8.37	87.42	1.42	0.15	0.00	0.00	29	NP	-	-	-	-	-	-	-
12.00	29	0.76	22.04	Silty Sand	3.25	7.83	87.56	0.99	0.37	0.00	0.00	30	NP	-	-	-	-	-	-	-



**CONSULTING
Engineers Group Ltd.**
PLOT NO. 10, INDUSTRIAL AREA, PHASE II, GATE NO. 1, Gurgaon, Haryana

DFCCIL KESARI TO SANEHWAL

BORELOG OF BH-1(LHS) AT EXISTING KM-358/1 FOR ALIGNMENT
ON KESARI TO SANEHWAL, LUDHIANA



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LEGEND

SYMBOL	DESCRIPTION
	SANDY SILT
	SILTY SAND

ANNEXURE - III

Calculation of SBC for shallow foundations as per IS : 6403 - 1981

INPUT DATA

	Alignment at Ch 358/1	BH-1
<i>Type of footing</i>		
1 Continuous Strip		
2 Rectangular	Rectangular	2
3 Square		
4 Circular		

Angle of internal friction (ϕ°)	26.00
Cohesion (c in t/m ²)	0.00
Void ratio (e)	0.59
Direction of load with vertical (ρ°)	0.00
Density of surcharge (t/m ³)	1.70
Density of foundation soil (t/m ³)	1.73
Depth of water table(m)	1.50
Factor of safety	3.00

S.no.	Depth (m)	Width (m)	Length (m)
1	1.50	3.00	8.00
2	3.00	3.00	8.00
3	4.50	3.00	8.00
4	6.00	3.00	8.00

SHEAR FAILURE CRITERIA

Assumptions and formula used in calculation as per IS:6403-1981 are given below -

The ultimate net bearing capacity in case of general shear failure is given by

$$q_d = c N_c s_c d_c i_c + q (N_q - 1) s_q d_q i_q + (1/2) B \gamma N_\gamma s_\gamma d_\gamma i_\gamma W'$$

The ultimate net bearing capacity in case of local shear failure is given by

$$q'_d = (2/3) c N'_c s'_c d'_c i'_c + q (N'_q - 1) s'_q d'_q i'_q + (1/2) B \gamma N'_\gamma s'_\gamma d'_\gamma i'_\gamma W'$$

Where,

$$d_c = 1 + 0.2 (D_f/B) * \text{SQRT}(N_q)$$

$$d_q = d_\gamma = 1 \text{ for } \phi < 10^\circ$$

$$d_q = d_\gamma = 1 + 0.1 (D_f/B) * \text{SQRT}(N_q) \text{ for } \phi > 10^\circ$$

$$N_\phi = \tan^2(\pi/4 + \phi/2)$$

$$\phi' \text{ for local shear failure} = \tan^{-1} (0.67 \tan \phi)$$

OUTPUT

The computer aided results for shear failure criteria are tabulated below. The results are interpolated values of bearing capacity obtained from general and local shear failure criteria.

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ANNEXURE - III

Bearing capacity factors :

ϕ	26.00	ϕ'	18.10
N_c	22.60	N'_c	13.36
N_q	12.21	N'_q	5.46
N_γ	13.18	N'_γ	4.35

Shape factors :

S.no.	Width(m)	Length (m)	S_c	S_q	S_γ
1	3.00	8.00	1.08	1.08	0.85
2	3.00	8.00	1.08	1.08	0.85
3	3.00	8.00	1.08	1.08	0.85
4	3.00	8.00	1.08	1.08	0.85

Depth factors :

S.no.	Depth(m)	Width(m)	d_c	d_q	d_γ
1	1.50	3.00	1.16	1.08	1.08
2	3.00	3.00	1.32	1.16	1.16
3	4.50	3.00	1.48	1.24	1.24
4	6.00	3.00	1.64	1.32	1.32

Inclination factors :

$i_c = (1 - \alpha / 90)^2$	$i_q = (1 - \alpha / 90)^2$	$i_\gamma = (1 - \alpha / \phi)^2$
1.00	1.00	1.00

Water table factor :

S.no.	Depth(m)	Width(m)	Z_w/B	W
1	1.50	3.00	0.00	0.50
2	3.00	3.00	-0.50	0.50
3	4.50	3.00	-1.00	0.50
4	6.00	3.00	-1.50	0.50

Safe Bearing Capacity

S.no.	Depth(m)	Width(m)	Length (m)	SBC in (t/m ²)		
				General shea	Local shear	Actual
1	1.50	3.00	8.00	16.30	6.13	14.26
2	3.00	3.00	8.00	29.38	11.32	25.77
3	4.50	3.00	8.00	31.41	12.10	27.55
4	6.00	3.00	8.00	33.44	12.88	29.32

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ANNEXURE - IV

Settlement Calculation As per IS 8009 (Part 1)	
Location	Alignment
Chainage	358/1
Bore Hole No.	1

Footing Depth (m)	1.50
SBC (t/m ²)	13.00
Average N value	17
Settlement for 10 t/m ² (mm)	18.00
Total Settlement (mm)	23.40
Depth Correction	0.91
Rigidity Correction	0.8
Corrected Total Settlement (mm)	17.0

Footing Depth (m)	3.00
SBC (t/m ²)	18.00
Average N value	17
Settlement for 10 t/m ² (mm)	18.00
Total Settlement (mm)	32.40
Depth Correction	0.83
Rigidity Correction	0.8
Corrected Total Settlement (mm)	21.5

Footing Depth (m)	4.50
SBC (t/m ²)	18.50
Average N value	17
Settlement for 10 t/m ² (mm)	18.00
Total Settlement (mm)	33.30
Depth Correction	0.74
Rigidity Correction	0.8
Corrected Total Settlement (mm)	19.7

Footing Depth (m)	6.00
SBC (t/m ²)	19.50
Average N value	17
Settlement for 10 t/m ² (mm)	18.00
Total Settlement (mm)	35.10
Depth Correction	0.68
Rigidity Correction	0.8
Corrected Total Settlement (mm)	19.1

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CHAPTER - 29

"Alignment"

Location - Existing Km. - 357/1

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29.1 LOCATION OF STRUCTURE:

Alignment at existing km 357/1.

29.2 BOREHOLE DESCRIPTIONS:

- (a) Location of Structure, Boreholes with RL shown in **FIGURE-1**.
- (b) Subsurface Characteristic of Soil/Rock shown in **ANNEXURE-I**.
- (c) Borelogs and sub soil profile shown in **ANNEXURE-II**.
- (d) Calculations of Safe Bearing Capacities in **ANNEXURE-III**.
- (e) Calculations of Probable Settlement in **ANNEXURE-IV**.
- (f) Depth of water Table $\geq 17.00\text{m}$ below EGL.

Subsurface profile at the site

BOREHOLE No.	Depth (m)	Type of Soil/Rock	Soil/Rock Characteristics
BH-1	0.00 to 1.50	Sandy Silt	Loose
	1.50 to 9.00	Silty Sand	Medium Dense
	9.00 to 12.00	Silty Sand with Gravels	Medium Dense
	Below 12.00	Silty Sand	Medium Dense

29.3 CHEMICAL ANALYSIS OF SOIL:

BOREHOLE		CHEMICAL PROPERTIES					
No.	Depth (m)	pH	Carbonate	Chlorides %	Sulphate %	Nitrate %	Salinity %
BH-1	3.00	8.30	0.002	0.0013	NIL	0.0008	0.019

29.4 DIFFERENTIAL FREE SWELL INDEX (DFS)

Bore Hole No.	Depth (m)	DFS Index in %
BH-1	3.00	NIL
	9.00	NIL

29.5 NET ALLOWABLE BEARING PRESSURE

Borehole No.	Depth from EGL (m)	Net Allowable Bearing Pressure (t/m^2)
BH-1	1.50	13.00
	3.00	19.00
	4.50	20.00
	6.00	20.50

29.6 CONCLUSIONS

- Subsurface Profiles indicates suitable Soil formation for foundations.

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29.7 RECOMMENDATIONS

(i)	<i>Type of foundation</i>	Open foundation
(ii)	<i>Depth of foundation below GL</i>	Below 2.00m from EGL

Note- The above recommendations are based on the field and laboratory tests conducted on the soil, and our experience in this regard. If the actual subsoil conditions during excavation for the foundation differ from the observations reported here, the design experts/consultants should be referred for suggestion, further investigations. However, the Depth and Type of foundation is to be decided by the structure designer depending upon the type of loading/structure and site conditions.

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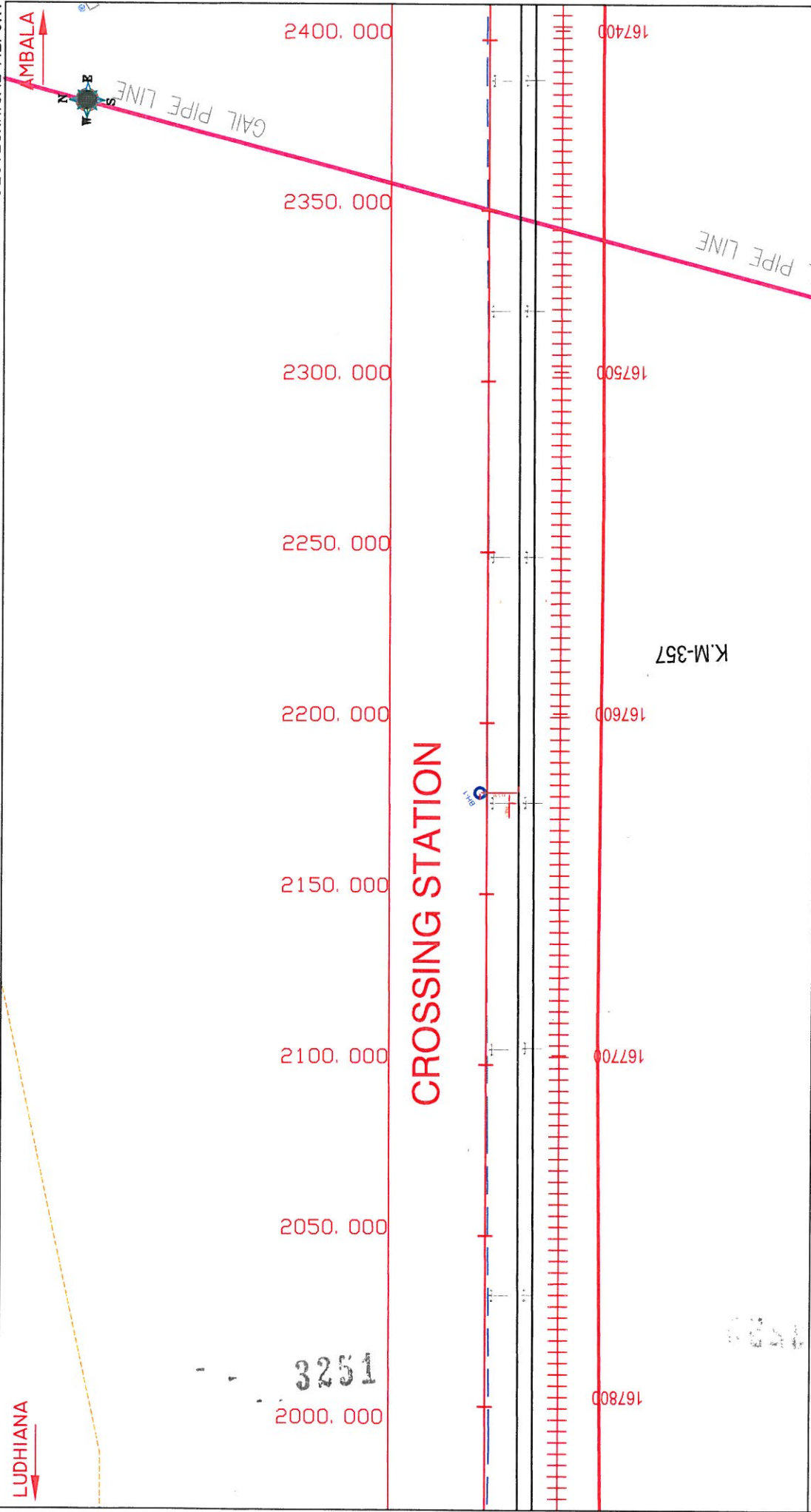


FIG.:-1 LOCATION PLAN OF PROPOSED ALIGNMENT AT CH. 357/1	PROJECT :- LUDHIANA-AMBALA (DFCCIL)	DESIGN :- CONSULTING ENGINEERS GROUP LTD. E-12, Meji Colony, Malviya Nagar, Jaipur-17 Tel: +91-141- 2520889, 2521899, 2520556 Fax: 2521348, E-Mail: ceg@cegroupindia.com
	ALL DIMENSIONS IN METER	

ANNEXURE - I

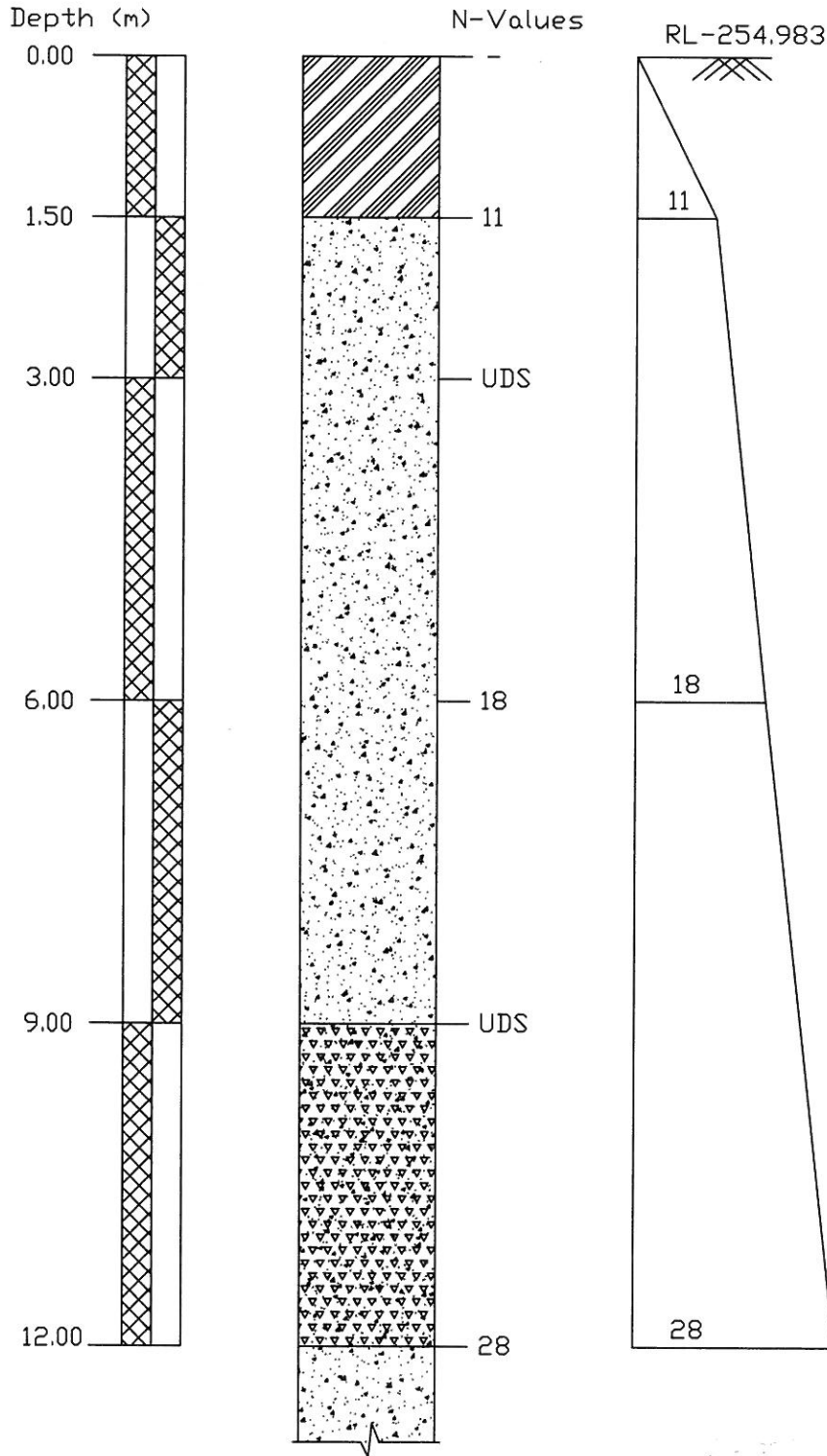
SOIL CHARACTERISTICS OF BORE HOLE AT BH-1 (LHS) OF ALIGNMENT AT CHAINAGE 357/1																					
Project :	Chainage 357/1			Date of Testing	Location at	B.H. No.	Depth of Water Table	Termination Depth			Surface Elevation										
	Observed	Correction	Corrected					Soil	Clay	Silt	Grain Size Distribution % wt retained	Atterberg Limits %	B.D.	M.C.	D.D.	Specific Gravity	Shear Strength				
Depth from (m)	N	C _n	N _h	Description (Soil Group)	Clay	Silt	Fine	Medium	Coarse	Fine	Coarse	L.L.	P.L.	P.I.	gm/cc	%	gm/cc	gm/cc	c	φ	
2.00	-	-	-	Sandy Silt	3.16	69.02	10.36	15.26	1.26	0.94	0.00	25	NP	NIL	-	-	-	-	-	-	-
1.50	11	1.46	16.06	Silty Sand	3.18	9.34	83.88	3.60	0.00	0.00	0.00	29	NP	NIL	-	-	-	-	-	-	-
3.00	UDS	-	-	Silty Sand	1.65	11.61	74.23	10.36	2.15	0.00	0.00	25	NP	NIL	1.68	4.69	1.60	2.66	0.00	27.00	-
6.00	18	1.00	18.00	Silty Sand	2.47	5.79	88.46	3.28	0.00	0.00	0.00	28	NP	NIL	-	-	-	-	-	-	-
9.00	UDS	-	-	Silty Sand with Gravels	3.67	14.35	71.21	1.23	1.12	8.42	0.00	26	NP	NIL	2.00	3.62	1.93	2.67	0.00	30.00	-
12.00	28	0.74	20.72	Silty Sand	2.97	11.27	82.98	2.65	0.13	0.00	0.00	27	NP	NIL	-	-	-	-	-	-	-



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DFCCIL KESARI TO SAMEHWAL

BORELOG OF BH-1(LHS) AT EXISTING KM-357/1 FOR ALIGNMENT
ON KESARI TO SANEHWAL, LUDHIANA



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LEGEND

SYMBOL	DESCRIPTION
	SANDY SILT
	SILTY SAND
	SILTY SAND WITH GRAVELS

ANNEXURE - III

Calculation of SBC for shallow foundations as per IS : 6403 - 1981

INPUT DATA

	Alignment at Ch 357/1	BH-1
<i>Type of footing</i>	Rectangular	2
1 Continuous Strip		
2 Rectangular		
3 Square		
4 Circular		
Angle of internal friction (ϕ°)		27.00
Cohesion (c in t/m ²)		0.00
Void ratio (e)		0.66
Direction of load with vertical ($\hat{\alpha}$)		0.00
Density of surcharge (t/m^3)		1.68
Density of foundation soil (t/m^3)		1.68
Depth of water table(m)		1.50
Factor of safety		3.00

S.no.	Depth (m)	Width (m)	Length (m)
1	1.50	3.00	8.00
2	3.00	3.00	8.00
3	4.50	3.00	8.00
4	6.00	3.00	8.00

SHEAR FAILURE CRITERIA

Assumptions and formula used in calculation as per IS:6403-1981 are given below -

The ultimate net bearing capacity in case of general shear failure is given by

$$q_d = c N_c s_c d_c i_c + q (N_q - 1) s_q d_q i_q + (1/2) B \gamma N_\gamma s_\gamma d_\gamma i_\gamma W'$$

The ultimate net bearing capacity in case of local shear failure is given by

$$q'_d = (2/3) c N'_c s_c d_c i_c + q (N'_q - 1) s_q d_q i_q + (1/2) B \gamma N'_\gamma s_\gamma d_\gamma i_\gamma W'$$

Where,

$$d_c = 1 + 0.2 (D_f/B) * \text{SQRT}(N_b)$$

$$d_q = d_\gamma = 1 \text{ for } \phi < 10^\circ$$

$$d_q = d_\gamma = 1 + 0.1 (D_f/B) * \text{SQRT}(N_b) \text{ for } \phi > 10^\circ$$

$$N_b = \tan^2(\pi/4 + \phi/2)$$

$$\phi' \text{ for local shear failure} = \tan^{-1} (0.67 \tan \phi)$$

OUTPUT

The computer aided results for shear failure criteria are tabulated below. The results are interpolated values of bearing capacity obtained from general and local shear failure criteria.

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ANNEXURE - III

Bearing capacity factors :

ϕ	27.00
N_c	24.49
N_q	13.76
N_γ	15.49

ϕ'	18.85
N'_c	13.94
N'_q	5.83
N'_γ	4.76

Shape factors :

S.no.	Width(m)	Length (m)	S_c	S_q	S_γ
1	3.00	8.00	1.08	1.08	0.85
2	3.00	8.00	1.08	1.08	0.85
3	3.00	8.00	1.08	1.08	0.85
4	3.00	8.00	1.08	1.08	0.85

Depth factors :

S.no.	Depth(m)	Width(m)	d_c	d_q	d_γ
1	1.50	3.00	1.16	1.08	1.08
2	3.00	3.00	1.33	1.16	1.16
3	4.50	3.00	1.49	1.24	1.24
4	6.00	3.00	1.65	1.33	1.33

Inclination factors :

$i_c = (1 - \alpha / 90)^2$	$i_q = (1 - \alpha / 90)^2$	$i_\gamma = (1 - \alpha / \phi)^2$
1.00	1.00	1.00

Water table factor :

S.no.	Depth(m)	Width(m)	Z_w/B	W
1	1.50	3.00	0.00	0.50
2	3.00	3.00	-0.50	0.50
3	4.50	3.00	-1.00	0.50
4	6.00	3.00	-1.50	0.50

Safe Bearing Capacity

S.no.	Depth(m)	Width(m)	Length (m)	SBC in (t/m^2)		
				General shear	Local shear	Actual
1	1.50	3.00	8.00	18.44	6.56	11.90
2	3.00	3.00	8.00	33.23	12.13	21.62
3	4.50	3.00	8.00	35.56	12.98	23.14
4	6.00	3.00	8.00	37.89	25.41	31.03

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ANNEXURE - IV

Settlement Calculation As per IS 8009 (Part 1)	
Location	Alignment
Chainage	357/1
Bore Hole No.	1

Footing Depth (m)	1.50
SBC (t/m ²)	13.00
Average N value	16
Settlement for 10 t/m ² (mm)	19.00
Total Settlement (mm)	24.70
Depth Correction	0.91
Rigidity Correction	0.8
Corrected Total Settlement (mm)	18.0

Footing Depth (m)	3.00
SBC (t/m ²)	19.00
Average N value	17
Settlement for 10 t/m ² (mm)	18.00
Total Settlement (mm)	34.20
Depth Correction	0.83
Rigidity Correction	0.8
Corrected Total Settlement (mm)	22.7

Footing Depth (m)	4.50
SBC (t/m ²)	20.00
Average N value	17
Settlement for 10 t/m ² (mm)	18.00
Total Settlement (mm)	36.00
Depth Correction	0.74
Rigidity Correction	0.8
Corrected Total Settlement (mm)	21.3

Footing Depth (m)	6.00
SBC (t/m ²)	20.50
Average N value	18
Settlement for 10 t/m ² (mm)	17.00
Total Settlement (mm)	34.85
Depth Correction	0.68
Rigidity Correction	0.8
Corrected Total Settlement (mm)	19.0

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CHAPTER - 30

"Alignment",

Location - Existing Km. - 356/1

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30.1 LOCATION OF STRUCTURE:

Alignment at existing km 356/1

30.2 BOREHOLE DESCRIPTIONS:

- Location of Structure, Boreholes with RL shown in **FIGURE-1**.
- Subsurface Characteristic of Soil/Rock shown in **ANNEXURE-I**.
- Borelogs and sub soil profile shown in **ANNEXURE-II**.
- Calculations of Safe Bearing Capacities in **ANNEXURE-III**.
- Calculations of Probable Settlement in **ANNEXURE-IV**.
- Depth of water Table $\geq 16.00\text{m}$ below EGL.

Subsurface profile at the site

BOREHOLE No.	Depth (m)	Type of Soil/Rock	Soil/Rock Characteristics
BH-1	0.00 to 1.50	Sandy Silt	Loose
	1.50 to 3.00	Silty Sand	Loose
	3.00 to 9.00	Silty Sand	Medium Dense
	9.00 to 12.00	Silty Sand with Gravels	Medium Dense
	Below 12.00	Silty Sand	Dense

30.3 CHEMICAL ANALYSIS OF SOIL:

BOREHOLE		CHEMICAL PROPERTIES					
No.	Depth (m)	pH	Carbonate	Chlorides %	Sulphate %	Nitrate %	Salinity %
BH-1	3.00	8.20	NIL	0.0011	NIL	0.0010	0.014

30.4 DIFFERENTIAL FREE SWELL INDEX (DFS)

Bore Hole No.	Depth (m)	DFS Index in %
BH-1	3.00	NIL

30.6 NET ALLOWABLE BEARING PRESSURE

Borehole No.	Depth from EGL (m)	Net Allowable Bearing Pressure (t/m^2)
BH-1	1.50	9.00
	3.00	15.00
	4.50	16.00
	6.00	20.00

30.7 CONCLUSIONS

- Subsurface Profiles indicates suitable Soil formation for foundations.

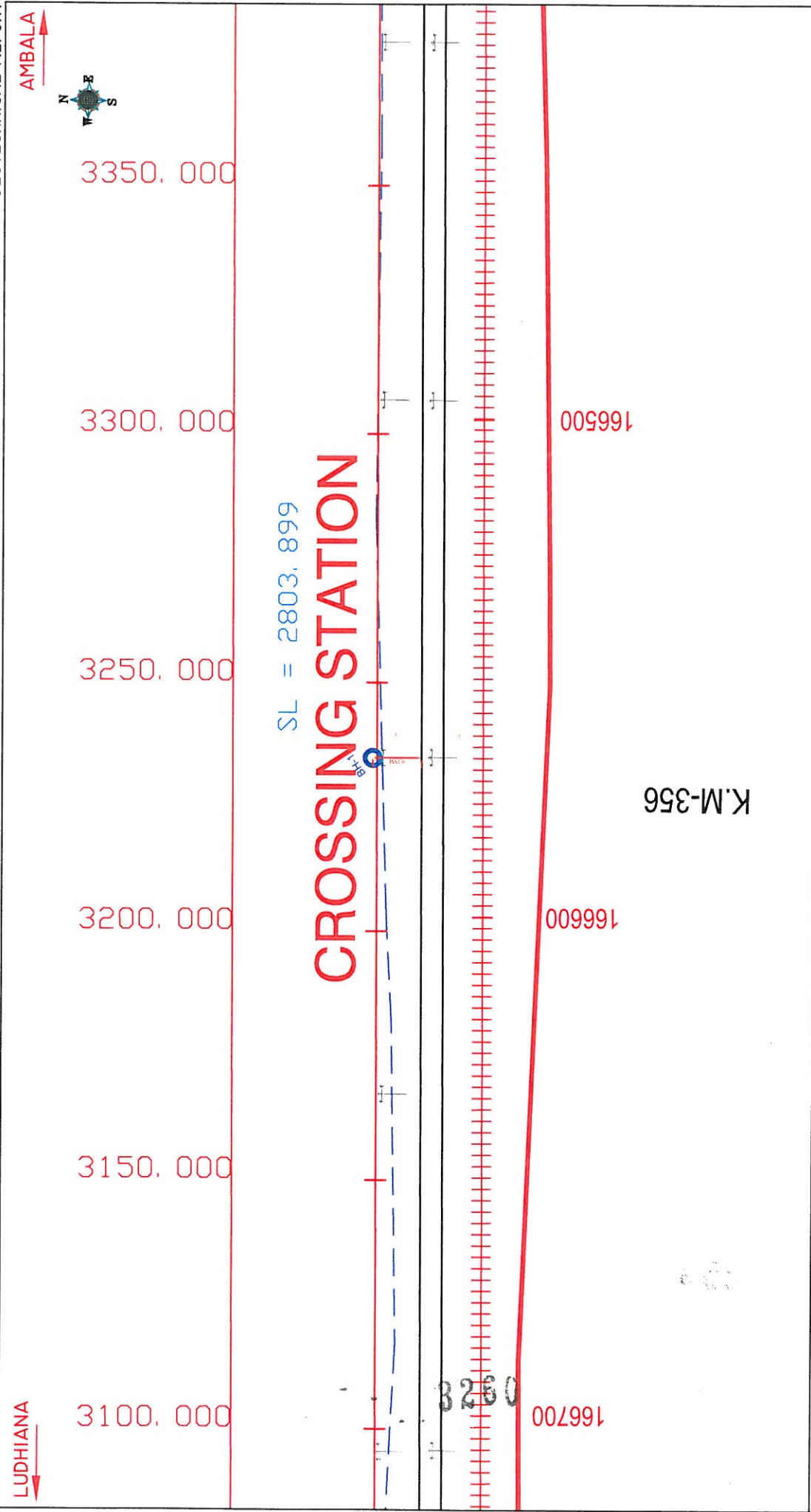
3258

30.8 RECOMMENDATIONS

(i)	<i>Type of foundation</i>	Open foundation
(ii)	<i>Depth of foundation below GL</i>	Below 3.00 m from EGL

Note- The above recommendations are based on the field and laboratory tests conducted on the soil, and our experience in this regard. If the actual subsoil conditions during excavation for the foundation differ from the observations reported here, the design experts/consultants should be referred for suggestion, further investigations. However, the Depth and Type of foundation is to be decided by the structure designer depending upon the type of loading/structure and site conditions.

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ALL DIMENSIONS IN METER FIG.:-1 LOCATION PLAN OF PROPOSED ALIGNMENT AT CH. 356/1	PROJECT :- LUDHIANA-AMBALA (DFCCIL)	DESIGN :- CONSULTING ENGINEERS GROUP LTD. E-12, Meji Colony, Malviya Nagar, Jaipur-17 Tel: +91-141-2520899, 2521899, 2520556 Fax: 2521348, E-Mail: ceg@cegroupindia.com
	RL OF BH-1 = 255.322	K.M-356 166600 166500

ANNEXURE - I

SOIL CHARACTERISTICS OF BORE HOLE AT BH-1 (LHS) OF ALIGNMENT AT CHAINAGE 356/1																				
Project :	Chainage 356/1			Date of Testing	Location at	B.H. No.	Depth of Water Table	Termination Depth			Surface Elevation			Ref. Code						
	Observed	Correction	Corrected					Soil	1	below 16.00 m.	12.00mtr	B.D.	M.C.		D.D.	Specific Gravity	Shear Strength			
Depth from GL (m)	N	C _n	N _n	Description (Soil Group)	Clay	Silt	Grain Size Distribution % wt retained			Atterberg Limits %			c kg/cm ²	φ degree						
							Fine	Medium	Coarse	Fine	Coarse	L.L.	P.L.	P.I.	gm/cc	%	gm/cc			
0.00	-	-	-	Sandy Silt	3.16	68.30	10.36	15.23	2.36	0.59	0.00	25	NIL	NP	-	-	-	-	-	-
1.50	7	1.43	10.01	Silty Sand	2.97	6.17	86.64	4.22	0.00	0.00	0.00	26	NIL	NP	-	-	-	-	-	-
3.00	UDS	-	-	Silty Sand	1.64	5.03	84.94	8.27	0.12	0.00	0.00	26	NIL	NP	1.86	6.25	1.75	2.67	0.00	28.50
6.00	14	0.97	13.58	Silty Sand	2.67	15.59	78.68	2.48	0.09	0.49	0.00	28	NIL	NP	-	-	-	-	-	-
9.00	29	0.83	24.07	Silty Sand with Gravels	3.28	7.46	79.74	2.60	0.29	6.63	0.00	27	NIL	NP	-	-	-	-	-	-
12.00	31	0.73	22.63	Silty Sand	2.14	5.67	89.90	2.29	0.00	0.00	0.00	29	NIL	NP	-	-	-	-	-	-

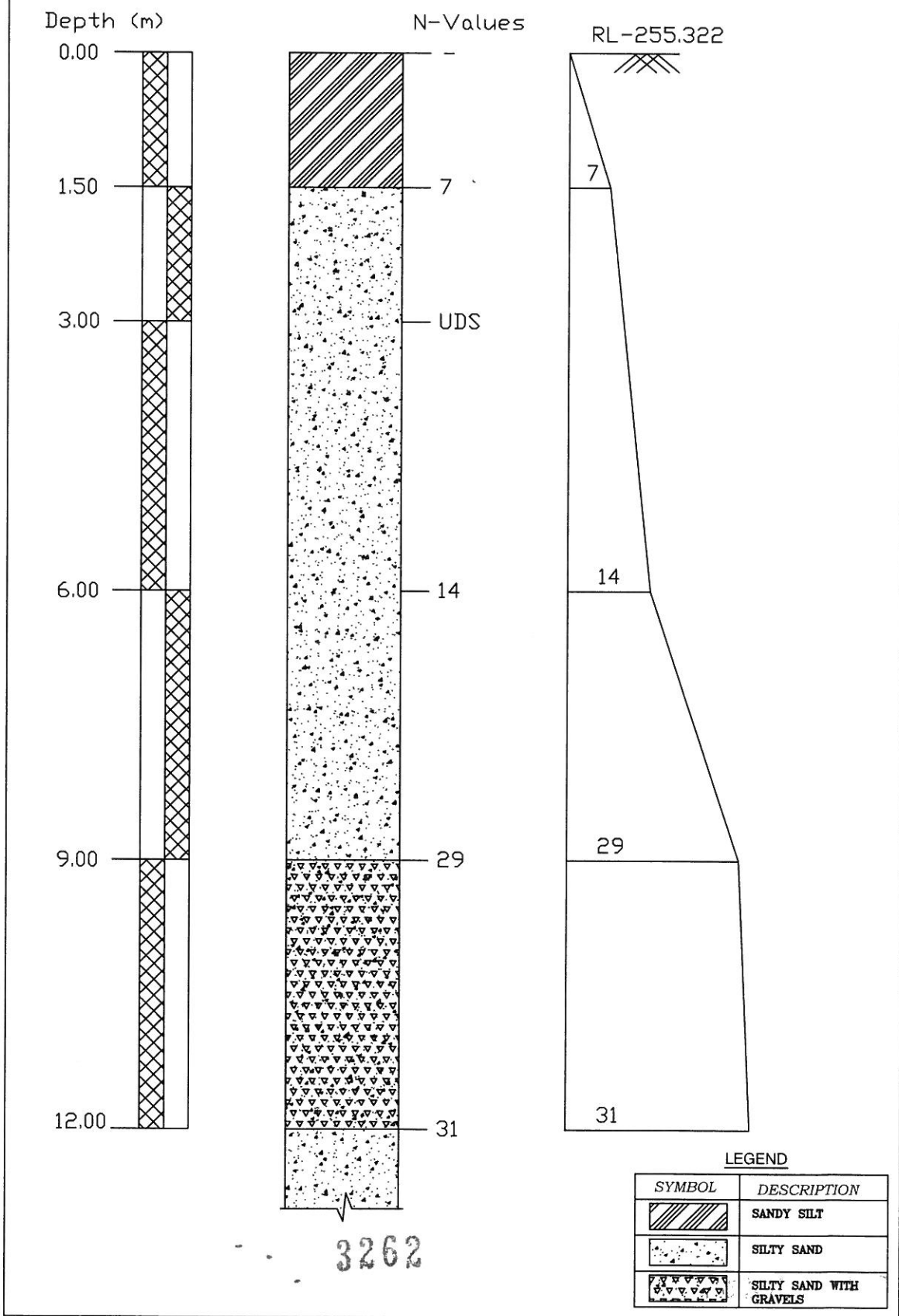


CONSULTING
Engineers Group Ltd.
101, 102, 103, 104, 105, 106, 107, 108, 109, 110, 111, 112, 113, 114, 115, 116, 117, 118, 119, 120, 121, 122, 123, 124, 125, 126, 127, 128, 129, 130, 131, 132, 133, 134, 135, 136, 137, 138, 139, 140, 141, 142, 143, 144, 145, 146, 147, 148, 149, 150, 151, 152, 153, 154, 155, 156, 157, 158, 159, 160, 161, 162, 163, 164, 165, 166, 167, 168, 169, 170, 171, 172, 173, 174, 175, 176, 177, 178, 179, 180, 181, 182, 183, 184, 185, 186, 187, 188, 189, 190, 191, 192, 193, 194, 195, 196, 197, 198, 199, 200, 201, 202, 203, 204, 205, 206, 207, 208, 209, 210, 211, 212, 213, 214, 215, 216, 217, 218, 219, 220, 221, 222, 223, 224, 225, 226, 227, 228, 229, 230, 231, 232, 233, 234, 235, 236, 237, 238, 239, 240, 241, 242, 243, 244, 245, 246, 247, 248, 249, 250, 251, 252, 253, 254, 255, 256, 257, 258, 259, 260, 261, 262, 263, 264, 265, 266, 267, 268, 269, 270, 271, 272, 273, 274, 275, 276, 277, 278, 279, 280, 281, 282, 283, 284, 285, 286, 287, 288, 289, 290, 291, 292, 293, 294, 295, 296, 297, 298, 299, 300, 301, 302, 303, 304, 305, 306, 307, 308, 309, 310, 311, 312, 313, 314, 315, 316, 317, 318, 319, 320, 321, 322, 323, 324, 325, 326, 327, 328, 329, 330, 331, 332, 333, 334, 335, 336, 337, 338, 339, 340, 341, 342, 343, 344, 345, 346, 347, 348, 349, 350, 351, 352, 353, 354, 355, 356, 357, 358, 359, 360, 361, 362, 363, 364, 365, 366, 367, 368, 369, 370, 371, 372, 373, 374, 375, 376, 377, 378, 379, 380, 381, 382, 383, 384, 385, 386, 387, 388, 389, 390, 391, 392, 393, 394, 395, 396, 397, 398, 399, 400, 401, 402, 403, 404, 405, 406, 407, 408, 409, 410, 411, 412, 413, 414, 415, 416, 417, 418, 419, 420, 421, 422, 423, 424, 425, 426, 427, 428, 429, 430, 431, 432, 433, 434, 435, 436, 437, 438, 439, 440, 441, 442, 443, 444, 445, 446, 447, 448, 449, 450, 451, 452, 453, 454, 455, 456, 457, 458, 459, 460, 461, 462, 463, 464, 465, 466, 467, 468, 469, 470, 471, 472, 473, 474, 475, 476, 477, 478, 479, 480, 481, 482, 483, 484, 485, 486, 487, 488, 489, 490, 491, 492, 493, 494, 495, 496, 497, 498, 499, 500, 501, 502, 503, 504, 505, 506, 507, 508, 509, 510, 511, 512, 513, 514, 515, 516, 517, 518, 519, 520, 521, 522, 523, 524, 525, 526, 527, 528, 529, 530, 531, 532, 533, 534, 535, 536, 537, 538, 539, 540, 541, 542, 543, 544, 545, 546, 547, 548, 549, 550, 551, 552, 553, 554, 555, 556, 557, 558, 559, 560, 561, 562, 563, 564, 565, 566, 567, 568, 569, 570, 571, 572, 573, 574, 575, 576, 577, 578, 579, 580, 581, 582, 583, 584, 585, 586, 587, 588, 589, 590, 591, 592, 593, 594, 595, 596, 597, 598, 599, 600, 601, 602, 603, 604, 605, 606, 607, 608, 609, 610, 611, 612, 613, 614, 615, 616, 617, 618, 619, 620, 621, 622, 623, 624, 625, 626, 627, 628, 629, 630, 631, 632, 633, 634, 635, 636, 637, 638, 639, 640, 641, 642, 643, 644, 645, 646, 647, 648, 649, 650, 651, 652, 653, 654, 655, 656, 657, 658, 659, 660, 661, 662, 663, 664, 665, 666, 667, 668, 669, 670, 671, 672, 673, 674, 675, 676, 677, 678, 679, 680, 681, 682, 683, 684, 685, 686, 687, 688, 689, 690, 691, 692, 693, 694, 695, 696, 697, 698, 699, 700, 701, 702, 703, 704, 705, 706, 707, 708, 709, 710, 711, 712, 713, 714, 715, 716, 717, 718, 719, 720, 721, 722, 723, 724, 725, 726, 727, 728, 729, 730, 731, 732, 733, 734, 735, 736, 737, 738, 739, 740, 741, 742, 743, 744, 745, 746, 747, 748, 749, 750, 751, 752, 753, 754, 755, 756, 757, 758, 759, 760, 761, 762, 763, 764, 765, 766, 767, 768, 769, 770, 771, 772, 773, 774, 775, 776, 777, 778, 779, 780, 781, 782, 783, 784, 785, 786, 787, 788, 789, 790, 791, 792, 793, 794, 795, 796, 797, 798, 799, 800, 801, 802, 803, 804, 805, 806, 807, 808, 809, 810, 811, 812, 813, 814, 815, 816, 817, 818, 819, 820, 821, 822, 823, 824, 825, 826, 827, 828, 829, 830, 831, 832, 833, 834, 835, 836, 837, 838, 839, 840, 841, 842, 843, 844, 845, 846, 847, 848, 849, 850, 851, 852, 853, 854, 855, 856, 857, 858, 859, 860, 861, 862, 863, 864, 865, 866, 867, 868, 869, 870, 871, 872, 873, 874, 875, 876, 877, 878, 879, 880, 881, 882, 883, 884, 885, 886, 887, 888, 889, 890, 891, 892, 893, 894, 895, 896, 897, 898, 899, 900, 901, 902, 903, 904, 905, 906, 907, 908, 909, 910, 911, 912, 913, 914, 915, 916, 917, 918, 919, 920, 921, 922, 923, 924, 925, 926, 927, 928, 929, 930, 931, 932, 933, 934, 935, 936, 937, 938, 939, 940, 941, 942, 943, 944, 945, 946, 947, 948, 949, 950, 951, 952, 953, 954, 955, 956, 957, 958, 959, 960, 961, 962, 963, 964, 965, 966, 967, 968, 969, 970, 971, 972, 973, 974, 975, 976, 977, 978, 979, 980, 981, 982, 983, 984, 985, 986, 987, 988, 989, 990, 991, 992, 993, 994, 995, 996, 997, 998, 999, 1000

DFCCIL KESARI TO SAMEHWAL

3261

BORELOG OF BH-1(LHS) AT EXISTING KM-356/1 FOR ALIGNMENT
ON KESARI TO SANEHWAL, LUDHIANA



LEGEND

SYMBOL	DESCRIPTION
	SANDY SILT
	SILTY SAND
	SILTY SAND WITH GRAVELS

ANNEXURE - III

Calculation of SBC for shallow foundations as per IS : 6403 - 1981

INPUT DATA

	Alignment at Ch 356/1	BH-1
<i>Type of footing</i>		
1 Continuous Strip		
2 Rectangular	Rectangular	2
3 Square		
4 Circular		
Angle of internal friction (ϕ°)		28.50
Cohesion (c in t/m ²)		0.00
Void ratio (e)		0.53
Direction of load with vertical ($^\circ$)		0.00
Density of surcharge (t/m ³)		1.70
Density of foundation soil (t/m ³)		1.86
Depth of water table(m)		1.50
Factor of safety		3.00

S.no.	Depth (m)	Width (m)	Length (m)
1	1.50	3.00	8.00
2	3.00	3.00	8.00
3	4.50	3.00	8.00
4	6.00	3.00	8.00

SHEAR FAILURE CRITERIA

Assumptions and formula used in calculation as per IS:6403-1981 are given below -

The ultimate net bearing capacity in case of general shear failure is given by

$$q_d = c N_c s_c d_c i_c + q (N_q - 1) s_q d_q i_q + (1/2) B \gamma N_\gamma s_\gamma d_\gamma i_\gamma W'$$

The ultimate net bearing capacity in case of local shear failure is given by

$$q'_d = (2/3) c N'_c s_c d_c i_c + q (N'_q - 1) s_q d_q i_q + (1/2) B \gamma N'_\gamma s_\gamma d_\gamma i_\gamma W'$$

Where,

$$d_c = 1 + 0.2 (D_f/B) * \text{SQRT}(N_\phi)$$

$$d_q = d_\gamma = 1 \text{ for } \phi < 10^\circ$$

$$d_q = d_\gamma = 1 + 0.1 (D_f/B) * \text{SQRT}(N_\phi) \text{ for } \phi > 10^\circ$$

$$N_\phi = \tan^2(\pi/4 + \phi/2)$$

$$\phi' \text{ for local shear failure} = \tan^{-1} (0.67 \tan \phi)$$

OUTPUT

The computer aided results for shear failure criteria are tabulated below. The results are interpolated values of bearing capacity obtained from general and local shear failure criteria.

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ANNEXURE - III

Bearing capacity factors :

ϕ	28.50
N_c	27.31
N_q	16.08
N_γ	18.94

ϕ'	19.99
N'_c	14.82
N'_q	6.40
N'_γ	5.38

Shape factors :

S.no.	Width(m)	Length (m)	S_c	S_q	S_γ
1	3.00	8.00	1.08	1.08	0.85
2	3.00	8.00	1.08	1.08	0.85
3	3.00	8.00	1.08	1.08	0.85
4	3.00	8.00	1.08	1.08	0.85

Depth factors :

S.no.	Depth(m)	Width(m)	d_c	d_q	d_γ
1	1.50	3.00	1.17	1.08	1.08
2	3.00	3.00	1.34	1.17	1.17
3	4.50	3.00	1.50	1.25	1.25
4	6.00	3.00	1.67	1.34	1.34

Inclination factors :

$i_c = (1 - \alpha / 90)^2$	$i_q = (1 - \alpha / 90)^2$	$i_\gamma = (1 - \alpha / \phi)^2$
1.00	1.00	1.00

Water table factor :

S.no.	Depth(m)	Width(m)	Z_w/B	W
1	1.50	3.00	0.00	0.50
2	3.00	3.00	-0.50	0.50
3	4.50	3.00	-1.00	0.50
4	6.00	3.00	-1.50	0.50

Safe Bearing Capacity

S.no.	Depth(m)	Width(m)	Length (m)	SBC in (t/m ²)		
				General shea	Local shear	Actual
1	1.50	3.00	8.00	23.05	7.65	23.05
2	3.00	3.00	8.00	40.93	14.00	40.93
3	4.50	3.00	8.00	43.88	15.01	43.88
4	6.00	3.00	8.00	46.82	29.19	46.82

ANNEXURE - IV

Settlement Calculation As per IS 8009 (Part 1)	
Location	Alignment
Chainage	356/1
Bore Hole No.	1

Footing Depth (m)	1.50
SBC (t/m ²)	9.00
Average N value	10
Settlement for 10 t/m ² (mm)	37.00
Total Settlement (mm)	33.30
Depth Correction	0.91
Rigidity Correction	0.8
Corrected Total Settlement (mm)	24.2

Footing Depth (m)	3.00
SBC (t/m ²)	15.00
Average N value	13
Settlement for 10 t/m ² (mm)	25.00
Total Settlement (mm)	37.50
Depth Correction	0.83
Rigidity Correction	0.8
Corrected Total Settlement (mm)	24.9

Footing Depth (m)	4.50
SBC (t/m ²)	16.00
Average N value	13
Settlement for 10 t/m ² (mm)	26.00
Total Settlement (mm)	41.60
Depth Correction	0.74
Rigidity Correction	0.8
Corrected Total Settlement (mm)	24.6

Footing Depth (m)	6.00
SBC (t/m ²)	20.00
Average N value	14
Settlement for 10 t/m ² (mm)	23.00
Total Settlement (mm)	46.00
Depth Correction	0.68
Rigidity Correction	0.8
Corrected Total Settlement (mm)	25.0

CHAPTER - 31

"Alignment",

Location - Existing Km. - 355/0-1

1036

31.1 LOCATION OF STRUCTURE:

Alignment at Span existing km 355/0-1

31.2 BOREHOLE DESCRIPTIONS:

- Location of Structure, Boreholes with RL shown in **FIGURE-1**.
- Subsurface Characteristic of Soil/Rock shown in **ANNEXURE-I**.
- Borelogs and sub soil profile shown in **ANNEXURE-II**.
- Calculations of Safe Bearing Capacities in **ANNEXURE-III**.
- Calculations of Probable Settlement in **ANNEXURE-IV**.
- Depth of water Table $\geq 17.00\text{m}$ below EGL.

Subsurface profile at the site

BOREHOLE No.	Depth (m)	Type of Soil/Rock	Soil/Rock Characteristics
BH-1	0.00 to 1.50	Sandy Silt	Loose
	1.50 to 3.00	Sandy Silt	Medium Dense
	3.00 to 4.50	Sandy Silt with Gravels	Medium Dense
	4.50 to 12.00	Silty Sand	Medium Dense
	Below 12.00	Silty Sand with Clay	Dense

31.3 CHEMICAL ANALYSIS OF SOIL:

BOREHOLE		CHEMICAL PROPERTIES					
No.	Depth (m)	pH	Carbonate %	Chlorides %	Sulphate %	Nitrate %	Salinity %
BH-1	3.00	8.70	0.005	0.0021	NIL	0.0010	0.042

31.4 DIFFERENTIAL FREE SWELL INDEX (DFS)

Bore Hole No.	Depth (m)	DFS Index in %
BH-1	3.00	NIL

31.6 NET ALLOWABLE BEARING PRESSURE

Borehole No.	Depth from EGL (m)	Net Allowable Bearing Pressure (t/m ²)
BH-1	1.50	20.00
	3.00	26.00
	4.50	26.50
	6.00	27.00

31.7 CONCLUSIONS

- Subsurface Profiles indicates suitable Soil formation for foundations.

3267

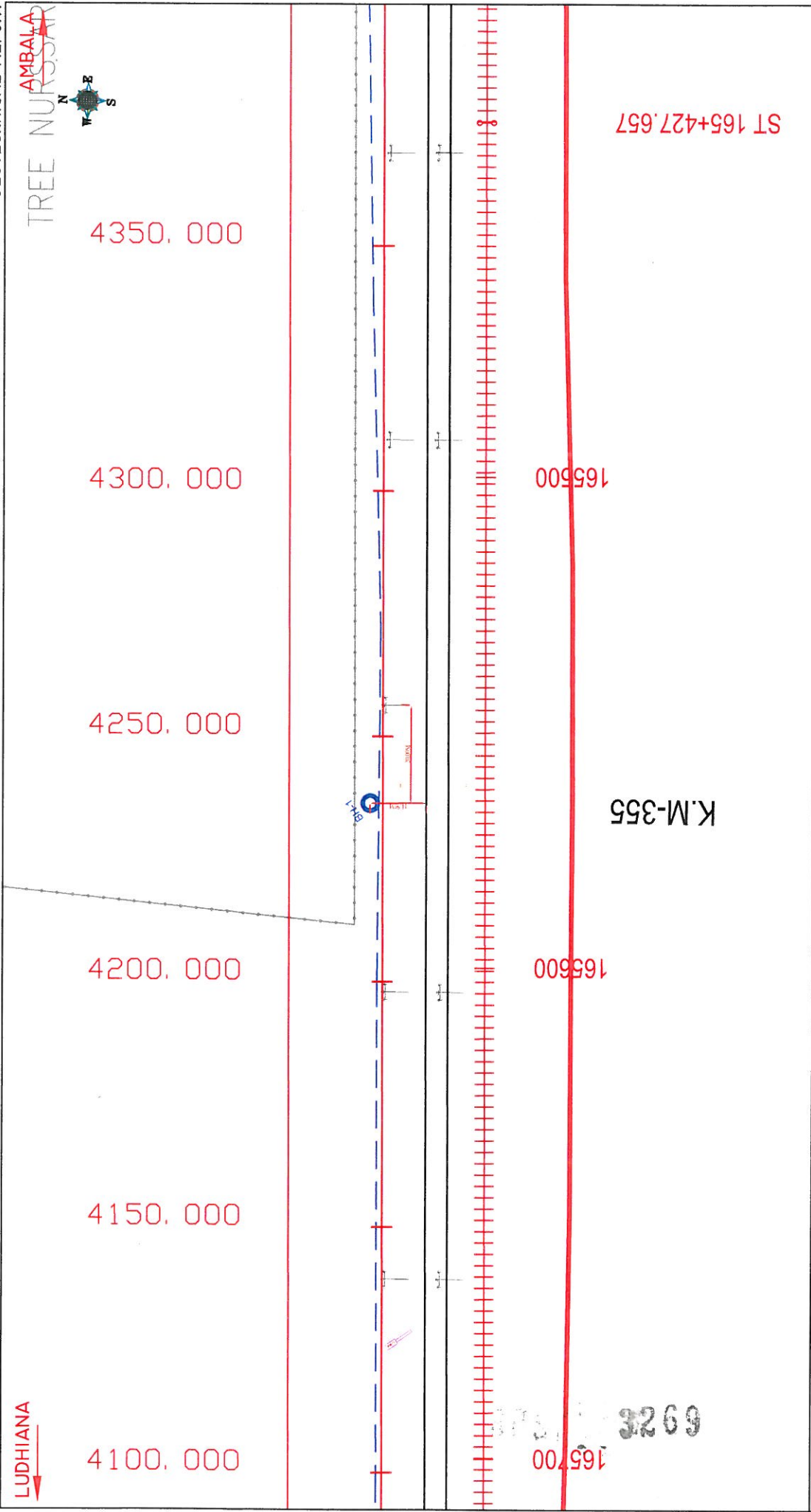
31.8 RECOMMENDATIONS

(i)	<i>Type of foundation</i>	Open foundation
(ii)	<i>Depth of foundation below GL</i>	Below 2.00m from EGL

Note- The above recommendations are based on the field and laboratory tests conducted on the soil, and our experience in this regard. If the actual subsoil conditions during excavation for the foundation differ from the observations reported here, the design experts/consultants should be referred for suggestion, further investigations. However, the Depth and Type of foundation is to be decided by the structure designer depending upon the type of loading/structure and site conditions.

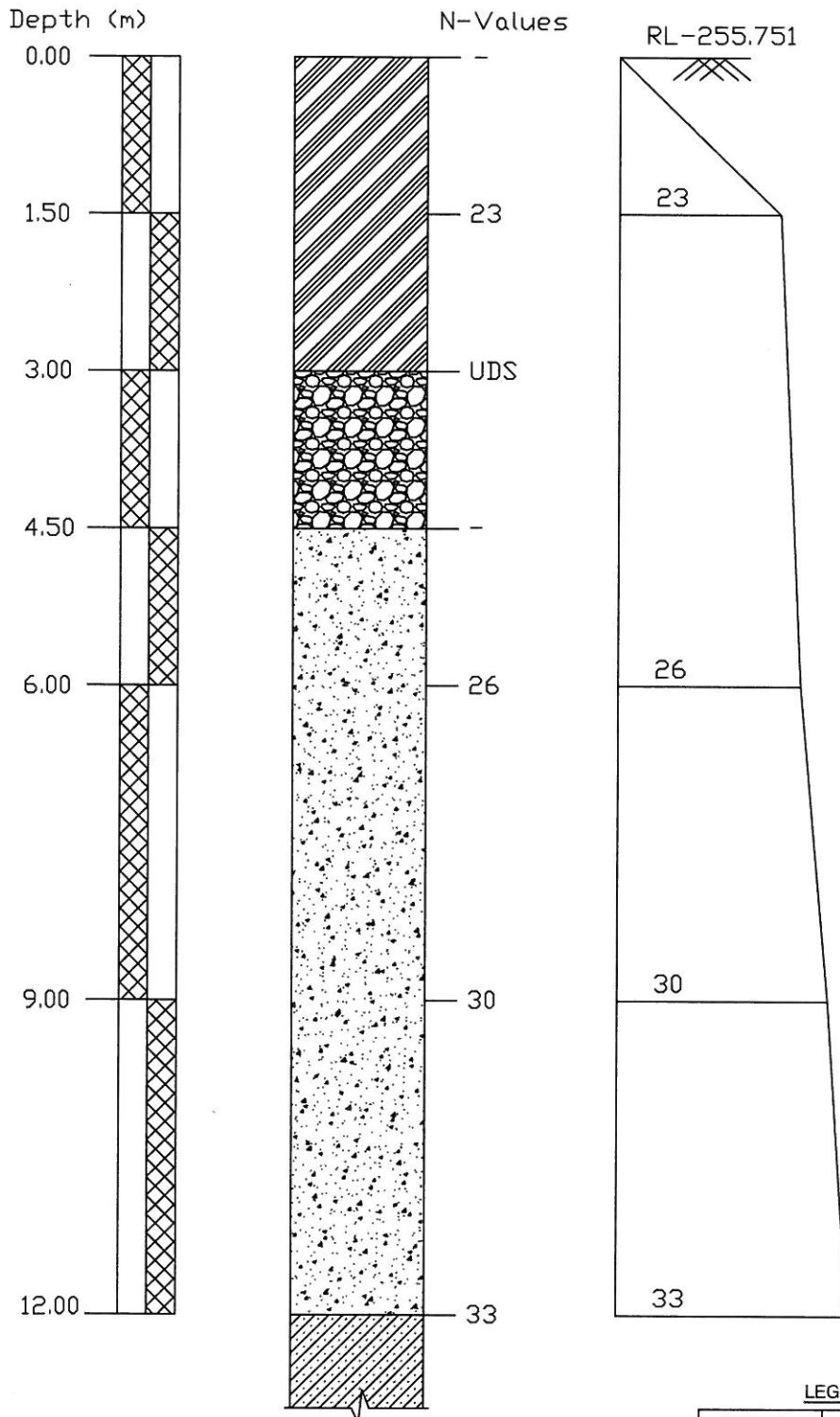
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LUDHIANA
 TREE NURSAR
 AMBALA



ALL DIMENSIONS IN METER FIG.-1 LOCATION PLAN OF PROPOSED ALIGNMENT AT CH. 355/0-1	PROJECT :- LUDHIANA-AMBALA (DFCCIL)	DESIGN :- CONSULTING ENGINEERS GROUP LTD E-12, Moji Colony, Malviya Nagar, Jaipur-17 Tel: +91-141- 2520899, 2521899, 2520556 Fax: 2521348, E-Mail: ceg@cegroupindia.com
	RL OF BH-1 = 255.751	ST 165+427.657

BORELOG OF BH-1(LHS) AT EXISTING KM-355/0-1 FOR ALIGNMENT
ON KESARI TO SANEHWAL, LUDHIANA



LEGEND

SYMBOL	DESCRIPTION
	SANDY SILT
	SANDY SILT WITH GRAVELS
	SILTY SAND
	SILTY SAND WITH CLAY

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ANNEXURE - III

Calculation of SBC for shallow foundations as per IS : 6403 - 1981

INPUT DATA

	Alignment at Ch 355/1	BH-1
<i>Type of footing</i>		
1 Continuous Strip		
2 Rectangular	Rectangular	2
3 Square		
4 Circular		
Angle of internal friction (ϕ°)		28.00
Cohesion (c in t/m ²)		0.00
Void ratio (e)		0.47
Direction of load with vertical ($^\circ$)		0.00
Density of surcharge (t/m ³)		1.70
Density of foundation soil (t/m ³)		1.87
Depth of water table(m)		1.50
Factor of safety		3.00

S.no.	Depth (m)	Width (m)	Length (m)
1	1.50	3.00	8.00
2	3.00	3.00	8.00
3	4.50	3.00	8.00
4	6.00	3.00	8.00

SHEAR FAILURE CRITERIA

Assumptions and formula used in calculation as per IS:6403-1981 are given below -

The ultimate net bearing capacity in case of general shear failure is given by

$$q_d = c N_c s_c d_c i_c + q (N_q - 1) s_q d_q i_q + (1/2) B \gamma N_\gamma s_\gamma d_\gamma i_\gamma W'$$

The ultimate net bearing capacity in case of local shear failure is given by

$$q'_d = (2/3) c N'_c s_c d_c i_c + q (N'_q - 1) s_q d_q i_q + (1/2) B \gamma N'_\gamma s_\gamma d_\gamma i_\gamma W'$$

Where,

$$d_c = 1 + 0.2 (D/B) * \text{SQRT}(N_\phi)$$

$$d_q = d_\gamma = 1 \text{ for } \phi < 10^\circ$$

$$d_q = d_\gamma = 1 + 0.1 (D/B) * \text{SQRT}(N_\phi) \text{ for } \phi > 10^\circ$$

$$N_\phi = \tan^2(\pi/4 + \phi/2)$$

$$\phi' \text{ for local shear failure} = \tan^{-1} (0.67 \tan \phi)$$

OUTPUT

The computer aided results for shear failure criteria are tabulated below. The results are interpolated values of bearing capacity obtained from general and local shear failure criteria.

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ANNEXURE - III

Bearing capacity factors :

ϕ	28.00
N_c	26.37
N_q	15.30
N_γ	17.79

ϕ'	19.61
N'_c	14.53
N'_q	6.21
N'_γ	5.18

Shape factors :

S.no.	Width(m)	Length (m)	S_c	S_q	S_γ
1	3.00	8.00	1.08	1.08	0.85
2	3.00	8.00	1.08	1.08	0.85
3	3.00	8.00	1.08	1.08	0.85
4	3.00	8.00	1.08	1.08	0.85

Depth factors :

S.no.	Depth(m)	Width(m)	d_c	d_q	d_γ
1	1.50	3.00	1.17	1.08	1.08
2	3.00	3.00	1.33	1.17	1.17
3	4.50	3.00	1.50	1.25	1.25
4	6.00	3.00	1.67	1.33	1.33

Inclination factors :

$i_c = (1 - \alpha / 90)^2$	$i_q = (1 - \alpha / 90)^2$	$i_\gamma = (1 - \alpha / \phi)^2$
1.00	1.00	1.00

Water table factor :

S.no.	Depth(m)	Width(m)	Z_w/B	W
1	1.50	3.00	0.00	0.50
2	3.00	3.00	-0.50	0.50
3	4.50	3.00	-1.00	0.50
4	6.00	3.00	-1.50	0.50

Safe Bearing Capacity

S.no.	Depth(m)	Width(m)	Length (m)	SBC in (t/m ²)		
				General shea	Local shear	Actual
1	1.50	3.00	8.00	21.82	7.38	21.82
2	3.00	3.00	8.00	38.74	13.50	38.74
3	4.50	3.00	8.00	41.50	14.46	41.50
4	6.00	3.00	8.00	44.27	15.42	44.27

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ANNEXURE - IV

Settlement Calculation As per IS 8009 (Part 1)	
Location	Alignment
Chainage	355/0-1
Bore Hole No.	1

Footing Depth (m)	1.50
SBC (t/m ²)	20.00
Average N value	28
Settlement for 10 t/m ² (mm)	10.00
Total Settlement (mm)	20.00
Depth Correction	0.91
Rigidity Correction	0.8
Corrected Total Settlement (mm)	14.6

Footing Depth (m)	3.30
SBC (t/m ²)	26.00
Average N value	25
Settlement for 10 t/m ² (mm)	12.00
Total Settlement (mm)	31.20
Depth Correction	0.83
Rigidity Correction	0.8
Corrected Total Settlement (mm)	20.7

Footing Depth (m)	4.50
SBC (t/m ²)	26.50
Average N value	25
Settlement for 10 t/m ² (mm)	12.00
Total Settlement (mm)	31.80
Depth Correction	0.74
Rigidity Correction	0.8
Corrected Total Settlement (mm)	18.8

Footing Depth (m)	6.00
SBC (t/m ²)	27.00
Average N value	25
Settlement for 10 t/m ² (mm)	12.00
Total Settlement (mm)	32.40
Depth Correction	0.68
Rigidity Correction	0.8
Corrected Total Settlement (mm)	17.6

3274

4752

CHAPTER - 32

"Alignment",

Location - Existing Km. - 347/1

3275

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32.1 LOCATION OF STRUCTURE:

Alignment at existing km 347/1

32.2 BOREHOLE DESCRIPTIONS:

- (a) Location of Structure, Boreholes with RL shown in **FIGURE-1**.
- (b) Subsurface Characteristic of Soil/Rock shown in **ANNEXURE-I**.
- (c) Borelogs and sub soil profile shown in **ANNEXURE-II**.
- (d) Calculations of Safe Bearing Capacities in **ANNEXURE-III**.
- (e) Calculations of Probable Settlement in **ANNEXURE-IV**.
- (f) Depth of water Table $\geq 14.00\text{m}$ below EGL.

Subsurface profile at the site

BOREHOLE No.	Depth (m)	Type of Soil/Rock	Soil/Rock Characteristics
BH-1	0.00 to 3.00	Silty Sand	Loose
	3.00 to 12.00	Silty Sand	Medium Dense
	Below 12.00	Silty Sand	Medium Dense

32.3 CHEMICAL ANALYSIS OF SOIL:

BOREHOLE		CHEMICAL PROPERTIES					
No.	Depth (m)	pH	Carbonate %	Chlorides %	Sulphate %	Nitrate %	Salinity %
BH-1	3.00	8.40	NIL	0.0011	NIL	0.0010	0.017

32.4 DIFFERENTIAL FREE SWELL INDEX (DFS)

Bore Hole No.	Depth (m)	DFS Index in %
BH-1	3.00	NIL
	9.00	NIL

32.5 NET ALLOWABLE BEARING PRESSURE

Borehole No.	Depth from EGL (m)	Net Allowable Bearing Pressure (t/m^2)
BH-1	1.50	9.00
	3.00	16.00
	4.50	17.00
	6.00	18.00

32.6 CONCLUSIONS

- Subsurface Profiles indicates suitable Soil formation for foundations.

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32.6 RECOMMENDATIONS

(i)	<i>Type of foundation</i>	Open foundation
(ii)	<i>Depth of foundation below GL</i>	Below 3.00m from EGL

Note- The above recommendations are based on the field and laboratory tests conducted on the soil, and our experience in this regard. If the actual subsoil conditions during excavation for the foundation differ from the observations reported here, the design experts/consultants should be referred for suggestion, further investigations. However, the Depth and Type of foundation is to be decided by the structure designer depending upon the type of loading/structure and site conditions.

3277

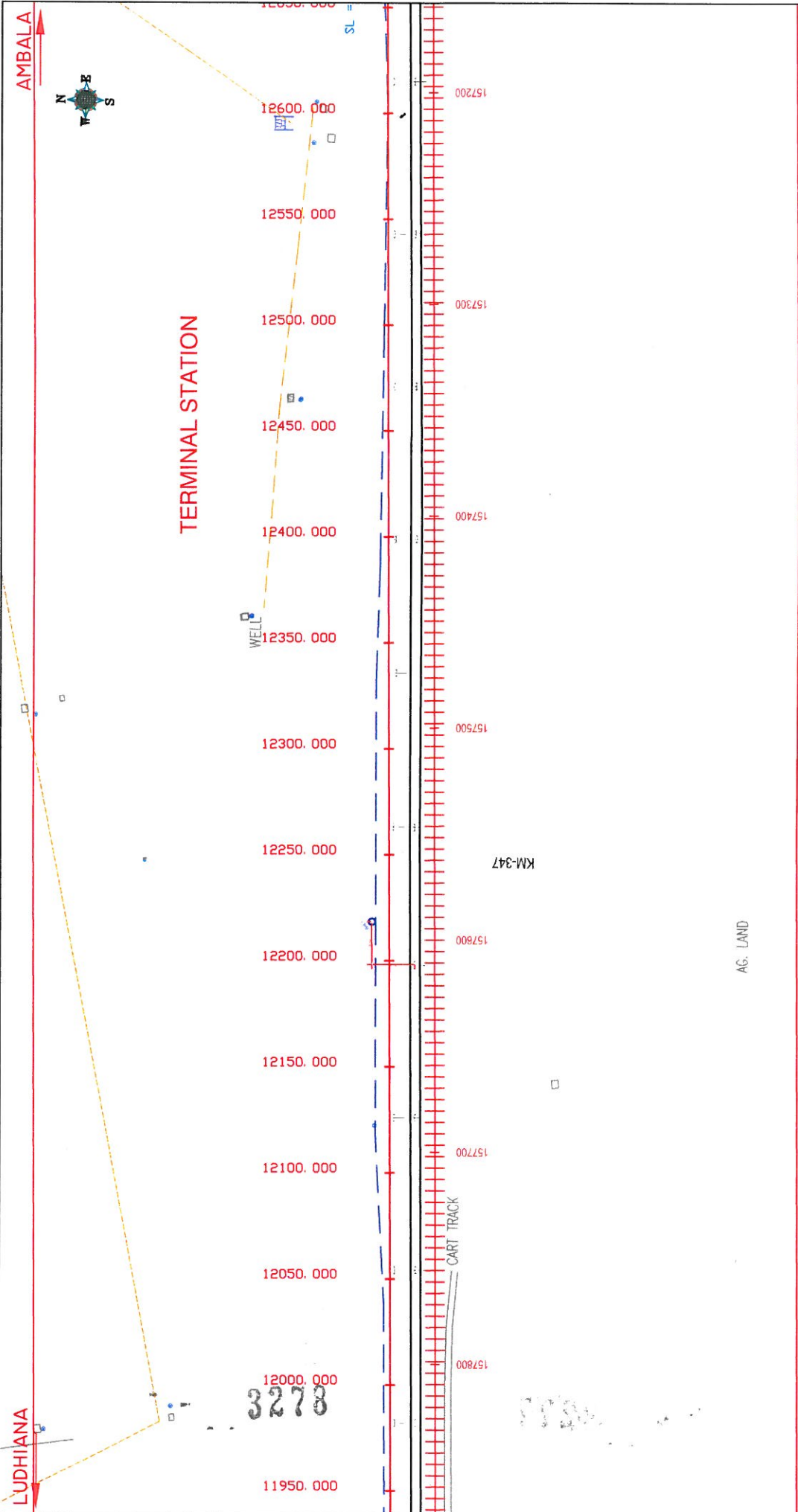


FIG:-1
 LOCATION PLAN OF PROPOSED ALIGNMENT
 AT CH. 347/1

PROJECT :-
 RL OF BH-1 = 257.916

DESIGN :-
 LUDHIANA-AMBALA (DFCCIL)

CONSULTING ENGINEERS GROUP LTD.
 E-12, Mohi Colony, Malviya Nagar, Jaipur-17
 Tel: +91-141-2520899, 2521899, 2520556
 Fax: 2521348, E-Mail: cegegindia.com

ANNEXURE - I

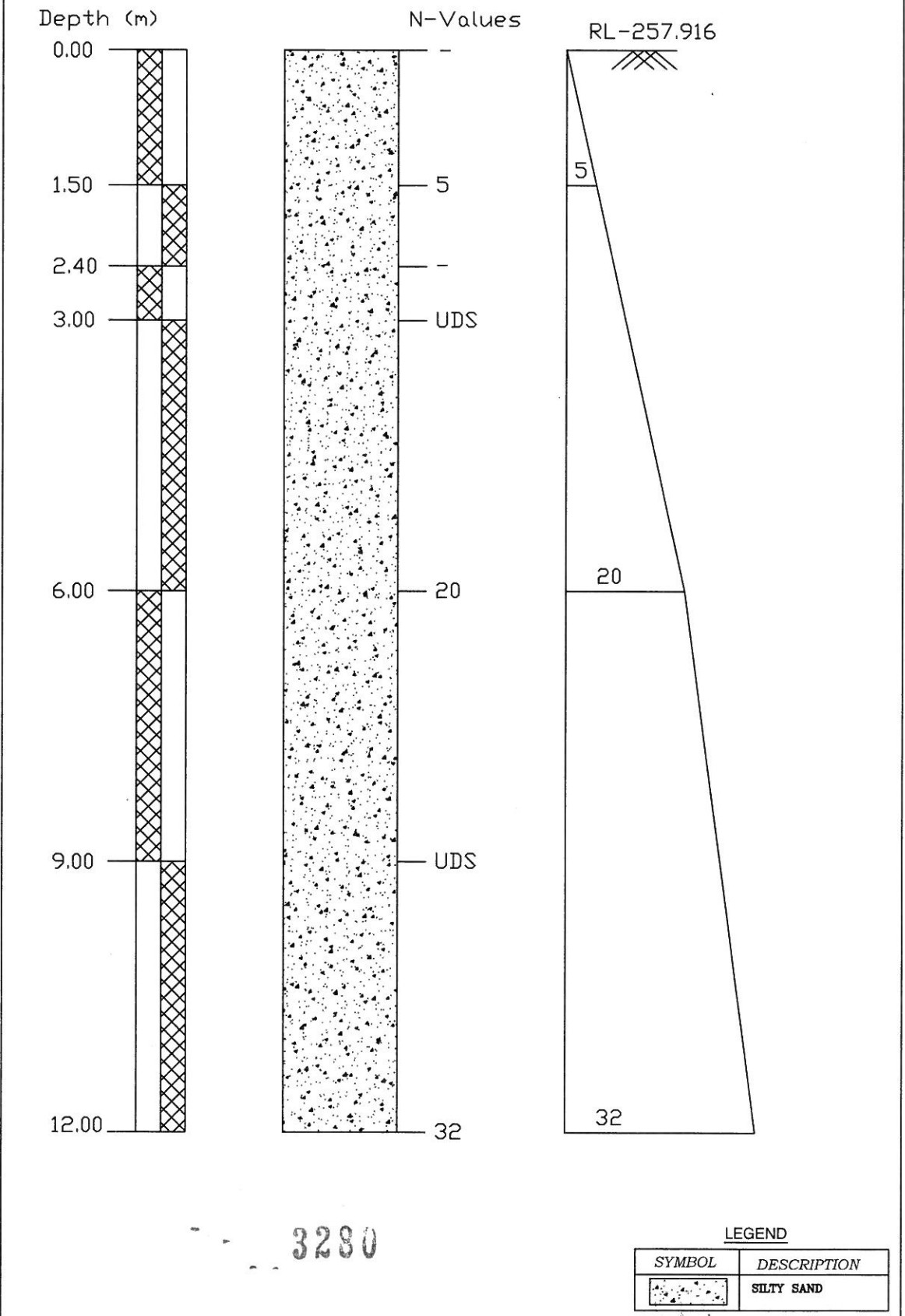
Geotechnical Report

SOIL CHARACTERISTICS OF BORE HOLE AT BH-I (LHS) OF ALIGNMENT AT CHAINAGE 347/1																						
Project :	Chainage 347/1			Date of Testing	Location at	B.H. No.	Depth of Water Table	Termination Depth			Surface Elevation			Ref. Code								
	Observed	Correction Factor	Corrected					Soil	Clay	Silt	Grain Size Distribution % wt retained	Atterberg Limits %	B.D.	M.C.	D.D.	Specific Gravity	Shear Strength					
Depth from GL (m)	N	C _n	N _n	Description (Soil Group)			Fine	Medium	Coarse	Fine	Coarse	Gravel	L.L.	P.L.	P.I.	gm/cc	%	gm/cc		c kg/cm ²	φ degree	
0.00	-	-	-	Silty Sand	3.17	34.37	50.36	10.65	1.45	0.00	0.00	0.00	22	NIL	NP	-	-	-	-	-	-	-
1.50	5	1.51	7.55	Silty Sand	2.67	39.35	56.59	1.39	0.00	0.00	0.00	0.00	23	NIL	NP	-	-	-	-	-	-	-
2.40				Silty Sand	2.56	16.69	65.29	14.23	1.23	0.00	0.00	0.00	24	NIL	NP	-	-	-	-	-	-	-
3.00	UDS	-	-	Silty Sand	2.16	6.21	88.52	3.01	0.10	0.00	0.00	0.00	27	NIL	NP	-	-	1.62	3.54	1.56	0.00	26.00
6.00	20	1.01	20.20	Silty Sand	1.85	8.41	87.68	2.06	0.00	0.00	0.00	0.00	24	NIL	NP	-	-	-	-	-	-	-
9.00	UDS	-	-	Silty Sand	2.67	10.22	84.21	2.45	0.45	0.00	0.00	0.00	27	NIL	NP	-	-	1.71	5.36	1.62	0.00	27.50
12.00	32	0.77	24.64	Silty Sand	3.11	7.28	87.20	2.41	0.00	0.00	0.00	0.00	24	NIL	NP	-	-	-	-	-	-	-



DFCCIL KESARI TO SAMEHWAL

BORELOG OF BH-1(LHS) AT EXISTING KM-347/1 FOR ALIGNMENT
ON KESARI TO SANEHWAL, LUDHIANA



ANNEXURE - III

Calculation of SBC for shallow foundations as per IS : 6403 - 1981

INPUT DATA

	Alignment at Ch 347/1	BH-1
Type of footing		
1 Continuous Strip		
2 Rectangular	Rectangular	2
3 Square		
4 Circular		

Angle of internal friction (ϕ°)	26.00
Cohesion (c in t/m ²)	0.00
Void ratio (e)	0.69
Direction of load with vertical (β°)	0.00
Density of surcharge (t/m ³)	1.62
Density of foundation soil (t/m ³)	1.62
Depth of water table(m)	1.50
Factor of safety	3.00

S. no.	Depth (m)	Width (m)	Length (m)
1	1.50	3.00	8.00
2	3.00	3.00	8.00
3	4.50	3.00	8.00
4	6.00	3.00	8.00

SHEAR FAILURE CRITERIA

Assumptions and formula used in calculation as per IS:6403-1981 are given below -

The ultimate net bearing capacity in case of general shear failure is given by

$$q_d = c N_c s_c d_c i_c + q (N_q - 1) s_q d_q i_q + (1/2) B \gamma N_\gamma s_\gamma d_\gamma i_\gamma W'$$

The ultimate net bearing capacity in case of local shear failure is given by

$$q_d = (2/3) c N'_c s_c d_c i_c + q (N'_q - 1) s_q d_q i_q + (1/2) B \gamma N'_\gamma s_\gamma d_\gamma i_\gamma W'$$

Where,

$$d_c = 1 + 0.2 (D/B) * \text{SQRT}(N_b)$$

$$d_q = d_\gamma = 1 \text{ for } \phi < 10^\circ$$

$$d_q = d_\gamma = 1 + 0.1 (D/B) * \text{SQRT}(N_b) \text{ for } \phi > 10^\circ$$

$$N_b = \tan^2(\pi/4 + \phi/2)$$

$$\phi' \text{ for local shear failure} = \tan^{-1} (0.67 \tan \phi)$$

OUTPUT

The computer aided results for shear failure criteria are tabulated below. The results are interpolated values of bearing capacity obtained from general and local shear failure criteria.

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ANNEXURE - III

Bearing capacity factors :

ϕ	26.00
N_c	22.60
N_q	12.21
N_γ	13.18

ϕ'	18.10
N'_c	13.36
N'_q	5.46
N'_γ	4.35

Shape factors :

S.no.	Width(m)	Length (m)	S_c	S_q	S_γ
1	3.00	8.00	1.08	1.08	0.85
2	3.00	8.00	1.08	1.08	0.85
3	3.00	8.00	1.08	1.08	0.85
4	3.00	8.00	1.08	1.08	0.85

Depth factors :

S.no.	Depth(m)	Width(m)	d_c	d_q	d_γ
1	1.50	3.00	1.16	1.08	1.08
2	3.00	3.00	1.32	1.16	1.16
3	4.50	3.00	1.48	1.24	1.24
4	6.00	3.00	1.64	1.32	1.32

Inclination factors :

$i_c = (1 - \alpha / 90)^2$	$i_q = (1 - \alpha / 90)^2$	$i_\gamma = (1 - \alpha / \phi)^2$
1.00	1.00	1.00

Water table factor :

S.no.	Depth(m)	Width(m)	Z_w/B	W'
1	1.50	3.00	0.00	0.50
2	3.00	3.00	-0.50	0.50
3	4.50	3.00	-1.00	0.50
4	6.00	3.00	-1.50	0.50

Safe Bearing Capacity

S.no.	Depth(m)	Width(m)	Length (m)	SBC in (t/m ²)		
				General shea	Local shear	Actual
1	1.50	3.00	8.00	15.44	5.81	8.70
2	3.00	3.00	8.00	27.91	10.75	15.90
3	4.50	3.00	8.00	29.83	11.49	17.00
4	6.00	3.00	8.00	31.76	12.24	18.09

3282

ANNEXURE - IV

Settlement Calculation As per IS 8009 (Part 1)	
Location	Alignment
Chainage	347/1
Bore Hole No.	1

Footing Depth (m)	1.50
SBC (t/m ²)	9.00
Average N value	12
Settlement for 10 t/m ² (mm)	29.00
Total Settlement (mm)	26.10
Depth Correction	0.91
Rigidity Correction	0.8
Corrected Total Settlement (mm)	19.0

Footing Depth (m)	3.00
SBC (t/m ²)	16.00
Average N value	15
Settlement for 10 t/m ² (mm)	21.00
Total Settlement (mm)	33.60
Depth Correction	0.83
Rigidity Correction	0.8
Corrected Total Settlement (mm)	22.3

Footing Depth (m)	4.50
SBC (t/m ²)	17.00
Average N value	16
Settlement for 10 t/m ² (mm)	19.00
Total Settlement (mm)	32.30
Depth Correction	0.74
Rigidity Correction	0.8
Corrected Total Settlement (mm)	19.1

Footing Depth (m)	6.00
SBC (t/m ²)	18.00
Average N value	20
Settlement for 10 t/m ² (mm)	15.00
Total Settlement (mm)	27.00
Depth Correction	0.68
Rigidity Correction	0.8
Corrected Total Settlement (mm)	14.7

3283

CHAPTER - 33

"Alignment",

Location - Existing Km. - 347/25-27

- - 3284 805

33.1 LOCATION OF STRUCTURE:

Alignment at existing km 347/25-27

33.2 BOREHOLE DESCRIPTIONS:

- Location of Structure, Boreholes with RL shown in **FIGURE-1**.
- Subsurface Characteristic of Soil/Rock shown in **ANNEXURE-I**.
- Borelogs and sub soil profile shown in **ANNEXURE-II**.
- Calculations of Safe Bearing Capacities in **ANNEXURE-III**.
- Calculations of Probable Settlement in **ANNEXURE-IV**.
- Depth of water Table $\geq 14.00\text{m}$ below EGL.

Subsurface profile at the site

BOREHOLE No.	Depth (m)	Type of Soil/Rock	Soil/Rock Characteristics
BH-1	0.00 to 1.50	Sandy Silt	Loose
	1.50 to 6.00	Sandy Silt	Medium Dense
	6.00 to 9.00	Sandy Silt with Gravels	Medium Dense
	9.00 to 12.00	Silty Sand	Medium Dense

33.3 CHEMICAL ANALYSIS OF SOIL:

BOREHOLE		CHEMICAL PROPERTIES					
No.	Depth (m)	pH	Carbonate %	Chlorides %	Sulphate %	Nitrate %	Salinity %
BH-1	6.00	8.70	0.012	0.0014	NIL	0.0009	0.019

33.4 DIFFERENTIAL FREE SWELL INDEX (DFS)

Bore Hole No.	Depth (m)	DFS Index in %
BH-1	6.00	NIL

33.5 NET ALLOWABLE BEARING PRESSURE

Borehole No.	Depth from EGL (m)	Net Allowable Bearing Pressure (t/m ²)
BH-1	1.50	9.50
	3.00	17.00
	4.50	18.00
	6.00	20.00

33.6 CONCLUSIONS

- Subsurface Profiles indicates suitable Soil formation for foundations.

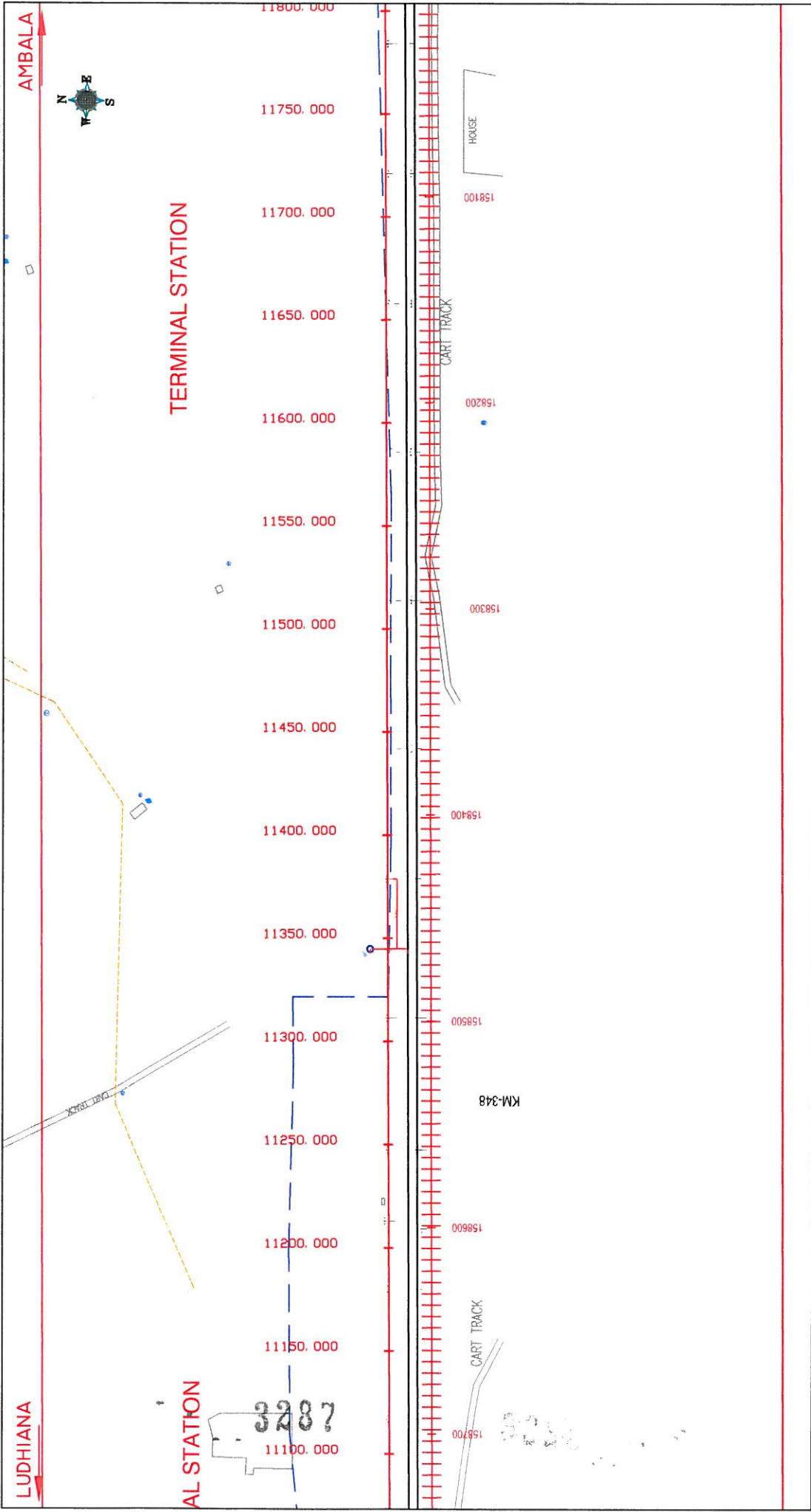
3205

33.7 RECOMMENDATIONS

(i)	<i>Type of foundation</i>	Open foundation
(ii)	<i>Depth of foundation below GL</i>	Below 3.00m from EGL

Note- The above recommendations are based on the field and laboratory tests conducted on the soil, and our experience in this regard. If the actual subsoil conditions during excavation for the foundation differ from the observations reported here, the design experts/consultants should be referred for suggestion, further investigations. However, the Depth and Type of foundation is to be decided by the structure designer depending upon the type of loading/structure and site conditions.

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<p>ALL DIMENSIONS IN METER</p>	<p>PROJECT :-</p>	<p>DESIGN :-</p>
<p>FIG :-1 LOCATION PLAN OF PROPOSED ALIGNMENT AT CH. 34.7/25-27</p>	<p>LUDHIANA-AMBALA (DFCCIL)</p>	<p>CONSULTING ENGINEERS GROUP LTD. E-12, Mohi Colony, Malviya Nagar, Jaipur-31 Tel: +91-141-2520899, 2521899, 2520556 Fax: 2521348, E-Mail: cege@ceginfolia.com</p>

ANNEXURE - I

SOIL CHARACTERISTICS OF BORE HOLE AT BH-1 (LHS) OF ALIGNMENT AT CHAINAGE 347/25-27																				
Project :	Chainage 347/25-27		Date of Testing		Location at		B.H. No.		Depth of Water Table		Termination Depth			Surface Elevation		Ref. Code				
	Observed	Correction Factor	Corrected	Soil Description (Soil Group)	Clay	Silt	Fine	Medium	Coarse	Fine	Coarse	L.L.	P.L.	P.I.	B.D.	M.C.	D.D.	Specific Gravity	Shear Strength	
Depth from GL (m)	N	C _n	N _n												gm/cc	%	gm/cc		c kg/cm ²	φ degree
0.00	-	-	-	Sandy Silt	3.26	76.68	11.38	5.26	1.23	2.19	0.00	24	NIL	NIL	-	-	-	-	-	-
1.50	11	1.52	16.72	Sandy Silt	2.97	83.22	8.02	1.04	1.88	2.87	0.00	25	NIL	NIL	-	-	-	-	-	-
3.00	17	1.25	21.25	Sandy Silt	3.18	89.71	6.25	0.55	0.10	0.21	0.00	33	NIL	NIL	-	-	-	-	-	-
6.00	UDS	-	-	Sandy Silt with Gravels	4.10	37.22	30.33	3.94	2.08	22.33	0.00	29	NIL	NIL	1.60	3.29	1.55	2.59	0.00	26.00
9.00	19	0.88	16.72	Silty Sand	2.13	30.57	50.22	4.67	8.29	4.12	0.00	22	NIL	NIL	-	-	-	-	-	-
12.00	27	0.78	18.03	Silty Sand	2.33	10.27	84.25	3.15	0.00	0.00	0.00	23	NIL	NIL	-	-	-	-	-	-

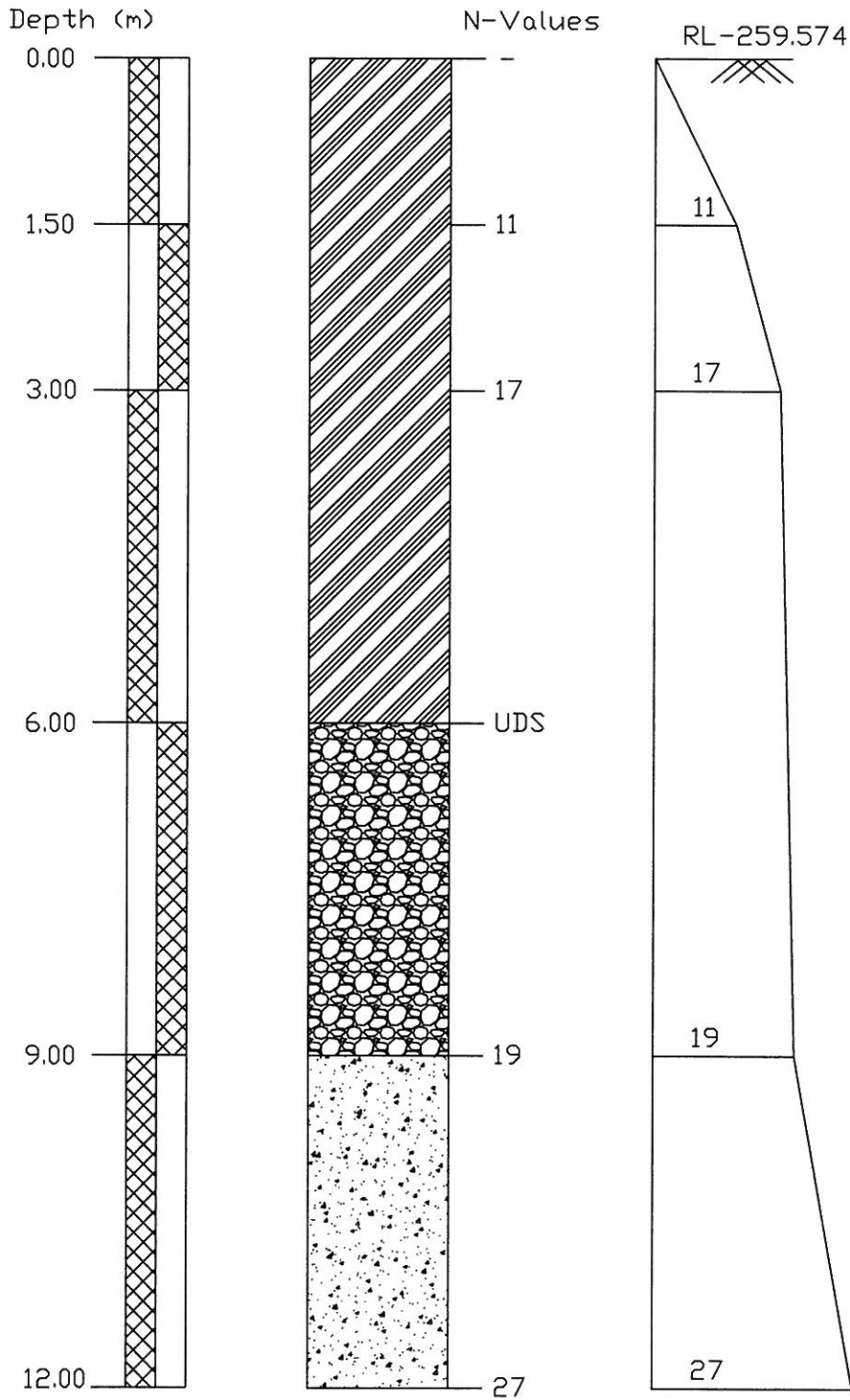


CONSULTING
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DFCCIL KESARI TO SANEHWAL

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BORELOG OF BH-1(LHS) AT EXISTING KM-347/25-27 FOR ALIGNMENT
ON KESARI TO SANEHWAL, LUDHIANA



LEGEND

SYMBOL	DESCRIPTION
	SANDY SILT
	SANDY SILT WITH GRAVELS
	SILTY SAND

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ANNEXURE - III

Calculation of SBC for shallow foundations as per IS : 6403 - 1981

INPUT DATA

	Alignment at Ch 347/25-27	BH-1
<i>Type of footing</i>		
1 Continuous Strip		
2 Rectangular	Rectangular	2
3 Square		
4 Circular		
Angle of internal friction (ϕ°)		26.00
Cohesion (c in t/m ²)		0.00
Void ratio (e)		0.67
Direction of load with vertical (β°)		0.00
Density of surcharge (t/m^3)		1.60
Density of foundation soil (t/m^3)		1.60
Depth of water table(m)		1.50
Factor of safety		3.00

S.no.	Depth (m)	Width (m)	Length (m)
1	1.50	3.00	8.00
2	3.00	3.00	8.00
3	4.50	3.00	8.00
4	6.00	3.00	8.00

SHEAR FAILURE CRITERIA

Assumptions and formula used in calculation as per IS:6403-1981 are given below -

The ultimate net bearing capacity in case of general shear failure is given by

$$q_u = c N_c s_c d_c i_c + q (N_q - 1) s_q d_q i_q + (1/2) B \gamma N_\gamma s_\gamma d_\gamma i_\gamma W'$$

The ultimate net bearing capacity in case of local shear failure is given by

$$q'_u = (2/3) c N'_c s_c d_c i_c + q (N'_q - 1) s_q d_q i_q + (1/2) B \gamma N'_\gamma s_\gamma d_\gamma i_\gamma W'$$

Where,

$$d_c = 1 + 0.2 (D/B) * \text{SQRT}(N_\phi)$$

$$d_q = d_\gamma = 1 \text{ for } \phi < 10^\circ$$

$$d_q = d_\gamma = 1 + 0.1 (D/B) * \text{SQRT}(N_\phi) \text{ for } \phi > 10^\circ$$

$$N_\phi = \tan^2(\pi/4 + \phi/2)$$

$$\phi' \text{ for local shear failure} = \tan^{-1} (0.67 \tan \phi)$$

OUTPUT

The computer aided results for shear failure criteria are tabulated below. The results are interpolated values of bearing capacity obtained from general and local shear failure criteria.

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ANNEXURE - III

Bearing capacity factors :

<table border="1" style="width: 100%; border-collapse: collapse;"> <tr><td>ϕ</td><td>26.00</td></tr> <tr><td>N_c</td><td>22.60</td></tr> <tr><td>N_q</td><td>12.21</td></tr> <tr><td>N_γ</td><td>13.18</td></tr> </table>	ϕ	26.00	N_c	22.60	N_q	12.21	N_γ	13.18	<table border="1" style="width: 100%; border-collapse: collapse;"> <tr><td>ϕ'</td><td>18.10</td></tr> <tr><td>N'_c</td><td>13.36</td></tr> <tr><td>N'_q</td><td>5.46</td></tr> <tr><td>N'_γ</td><td>4.35</td></tr> </table>	ϕ'	18.10	N'_c	13.36	N'_q	5.46	N'_γ	4.35
ϕ	26.00																
N_c	22.60																
N_q	12.21																
N_γ	13.18																
ϕ'	18.10																
N'_c	13.36																
N'_q	5.46																
N'_γ	4.35																

Shape factors :

S.no.	Width(m)	Length (m)	S_c	S_q	S_γ
1	3.00	8.00	1.08	1.08	0.85
2	3.00	8.00	1.08	1.08	0.85
3	3.00	8.00	1.08	1.08	0.85
4	3.00	8.00	1.08	1.08	0.85

Depth factors :

S.no.	Depth(m)	Width(m)	d_c	d_q	d_γ
1	1.50	3.00	1.16	1.08	1.08
2	3.00	3.00	1.32	1.16	1.16
3	4.50	3.00	1.48	1.24	1.24
4	6.00	3.00	1.64	1.32	1.32

Inclination factors :

$i_c = (1 - \alpha / 90)^2$	$i_q = (1 - \alpha / 90)^2$	$i_\gamma = (1 - \alpha / \phi)^2$
1.00	1.00	1.00

Water table factor :

S.no.	Depth(m)	Width(m)	Z_w/B	W'
1	1.50	3.00	0.00	0.50
2	3.00	3.00	-0.50	0.50
3	4.50	3.00	-1.00	0.50
4	6.00	3.00	-1.50	0.50

Safe Bearing Capacity

S.no.	Depth(m)	Width(m)	Length (m)	SBC in (t/m ²)		
				General shea	Local shear	Actual
1	1.50	3.00	8.00	15.25	5.74	9.55
2	3.00	3.00	8.00	27.56	10.62	17.40
3	4.50	3.00	8.00	29.46	11.35	18.60
4	6.00	3.00	8.00	31.37	12.09	19.80

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ANNEXURE - IV

Settlement Calculation As per IS 8009 (Part 1)	
Location	Alignment
Chainage	347/25-27
Bore Hole No.	1

Footing Depth (m)	1.50
SBC (t/m ²)	9.50
Average N value	18
Settlement for 10 t/m ² (mm)	17.00
Settlement (mm) for SBC	16.15
Depth Correction	0.91
Rigidity Correction	0.8
Corrected Total Settlement (mm)	11.8

Footing Depth (m)	3.00
SBC (t/m ²)	17.00
Average N value	19
Settlement for 10 t/m ² (mm)	16.00
Settlement (mm) for SBC	27.20
Depth Correction	0.83
Rigidity Correction	0.8
Corrected Total Settlement (mm)	18.1

Footing Depth (m)	4.50
SBC (t/m ²)	18.00
Average N value	18
Settlement for 10 t/m ² (mm)	18.00
Settlement (mm) for SBC	32.40
Depth Correction	0.74
Rigidity Correction	0.8
Corrected Total Settlement (mm)	19.2

Footing Depth (m)	6.00
SBC (t/m ²)	20.00
Average N value	16
Settlement for 10 t/m ² (mm)	20.00
Settlement (mm) for SBC	40.00
Depth Correction	0.68
Rigidity Correction	0.8
Corrected Total Settlement (mm)	21.8

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CHAPTER - 34

"Alignment",

Location - Existing Km. - 346/1

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34.1 LOCATION OF STRUCTURE:

Alignment at existing km 346/1

34.2 BOREHOLE DESCRIPTIONS:

- (a) Location of Structure, Boreholes with RL shown in **FIGURE-1**.
- (b) Subsurface Characteristic of Soil/Rock shown in **ANNEXURE-I**.
- (c) Borelogs and sub soil profile shown in **ANNEXURE-II**.
- (d) Calculations of Safe Bearing Capacities in **ANNEXURE-III**.
- (e) Calculations of Probable Settlement in **ANNEXURE-IV**.
- (f) Depth of water Table $\geq 16.00\text{m}$ below EGL.

Subsurface profile at the site

BOREHOLE No.	Depth (m)	Type of Soil/Rock	Soil/Rock Characteristics
BH-1	0.00 to 1.50	Silty Sand	Loose
	1.50 to 9.00	Silty Sand	Medium Dense
	9.00 to 12.00	Silty Sand	Dense

34.3 CHEMICAL ANALYSIS OF SOIL:

BOREHOLE		CHEMICAL PROPERTIES					
No.	Depth (m)	pH	Carbonate %	Chlorides %	Sulphate %	Nitrate %	Salinity %
BH-1	3.00	9.00	0.012	0.0014	NIL	0.0012	0.030

34.4 DIFFERENTIAL FREE SWELL INDEX (DFS)

Bore Hole No.	Depth (m)	DFS Index in %
BH-1	3.00	NIL

34.5 NET ALLOWABLE BEARING PRESSURE

Borehole No.	Depth from EGL (m)	Net Allowable Bearing Pressure (t/m^2)
BH-1	1.50	9.00
	3.00	16.00
	4.50	17.50
	6.00	19.00

34.6 CONCLUSIONS

- Subsurface Profiles indicates suitable Soil formation for foundations.

3294

34.7 RECOMMENDATIONS

(i)	<i>Type of foundation</i>	Open foundation
(ii)	<i>Depth of foundation below GL</i>	Below 3.00m from EGL

Note- The above recommendations are based on the field and laboratory tests conducted on the soil, and our experience in this regard. If the actual subsoil conditions during excavation for the foundation differ from the observations reported here, the design experts/consultants should be referred for suggestion, further investigations. However, the Depth and Type of foundation is to be decided by the structure designer depending upon the type of loading/structure and site conditions.

3295

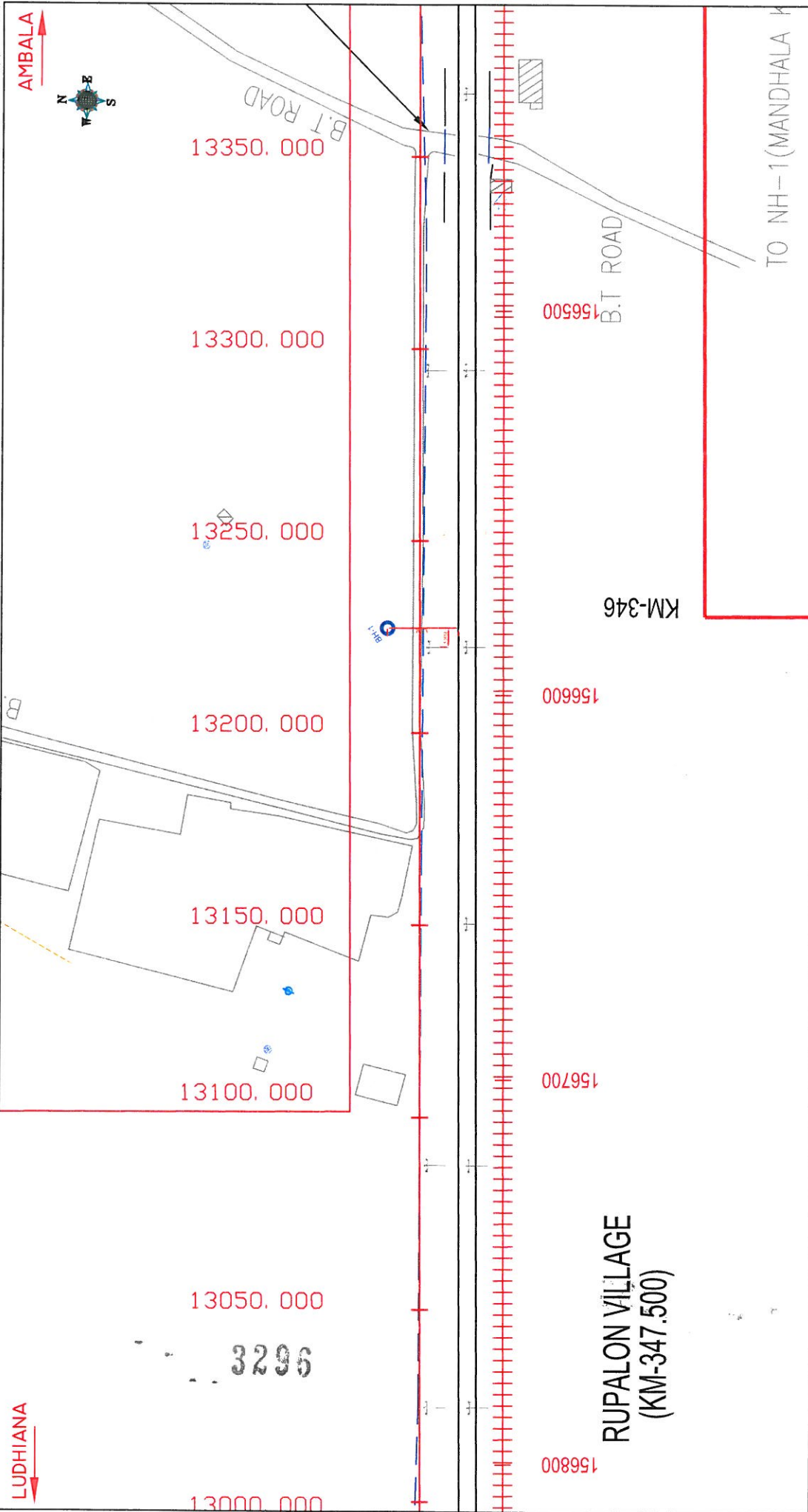


FIG.:-1 LOCATION PLAN OF PROPOSED ALIGNMENT AT CH. 346/1	PROJECT :- LUDHIANA-AMBALA (DFCCIL)	DESIGN :- CONSULTING ENGINEERS GROUP LTD. E-12, Maji Colony, Malviya Nagar, Jaipur-17 Tel: +91-141-2520899, 2521899, 2520556 Fax: 2521348, E-Mail: ceg@cegroupindia.com
	RL OF BH-1 = 261.885	TO NH-1 (MANDHALA K

ANNEXURE - I

SOIL CHARACTERISTICS OF BORE HOLE AT BH-1 (LHS) OF ALIGNMENT AT CHAINAGE 346/1																		
Project :	Chainage 346/1			Date of Testing		Location at	B.H. No.	Depth of Water Table		Termination Depth			Surface Elevation			Ref. Code		
	Observed	Correction Factor	Corrected	31.05.2009 to 31.05.2009	1			1 (LHS)	below 16.00 m.	12.00mtr	B.D.	M.C.	D.D.	B.D.	M.C.		D.D.	
Depth from GL (m)	N	C _n	N _n	Soil		Clay	Silt	Grain Size Distribution % wt retained			Atterberg Limits %			Specific Gravity	Shear Strength			
				Description (Soil Group)					Fine	Medium	Coarse	L.L.	P.L.		P.I.	gm/cc	%	gm/cc
0.00	-	-	-	Silty Sand	1.46	22.21	60.36	12.36	0.94	2.67	0.00	22	NIL	-	-	-	-	-
1.50	9	1.46	13.14	Silty Sand	1.37	21.41	73.86	2.53	0.83	0.00	24	NIL	NF	-	-	-	-	-
3.00	UDS	-	-	Silty Sand	3.67	7.77	76.46	4.97	2.19	4.94	29	NIL	NP	1.69	9.76	1.54	0.00	26.00
6.00	25	1.00	25.00	Silty Sand	2.48	7.43	81.92	2.74	1.06	4.37	27	NIL	NP	-	-	-	-	-
9.00	26	0.86	22.36	Silty Sand	2.59	6.12	83.62	4.64	0.50	2.53	25	NIL	NP	-	-	-	-	-
12.00	37	0.77	21.75	Silty Sand	2.21	8.31	84.23	4.58	0.58	0.09	25	NIL	NP	-	-	-	-	-

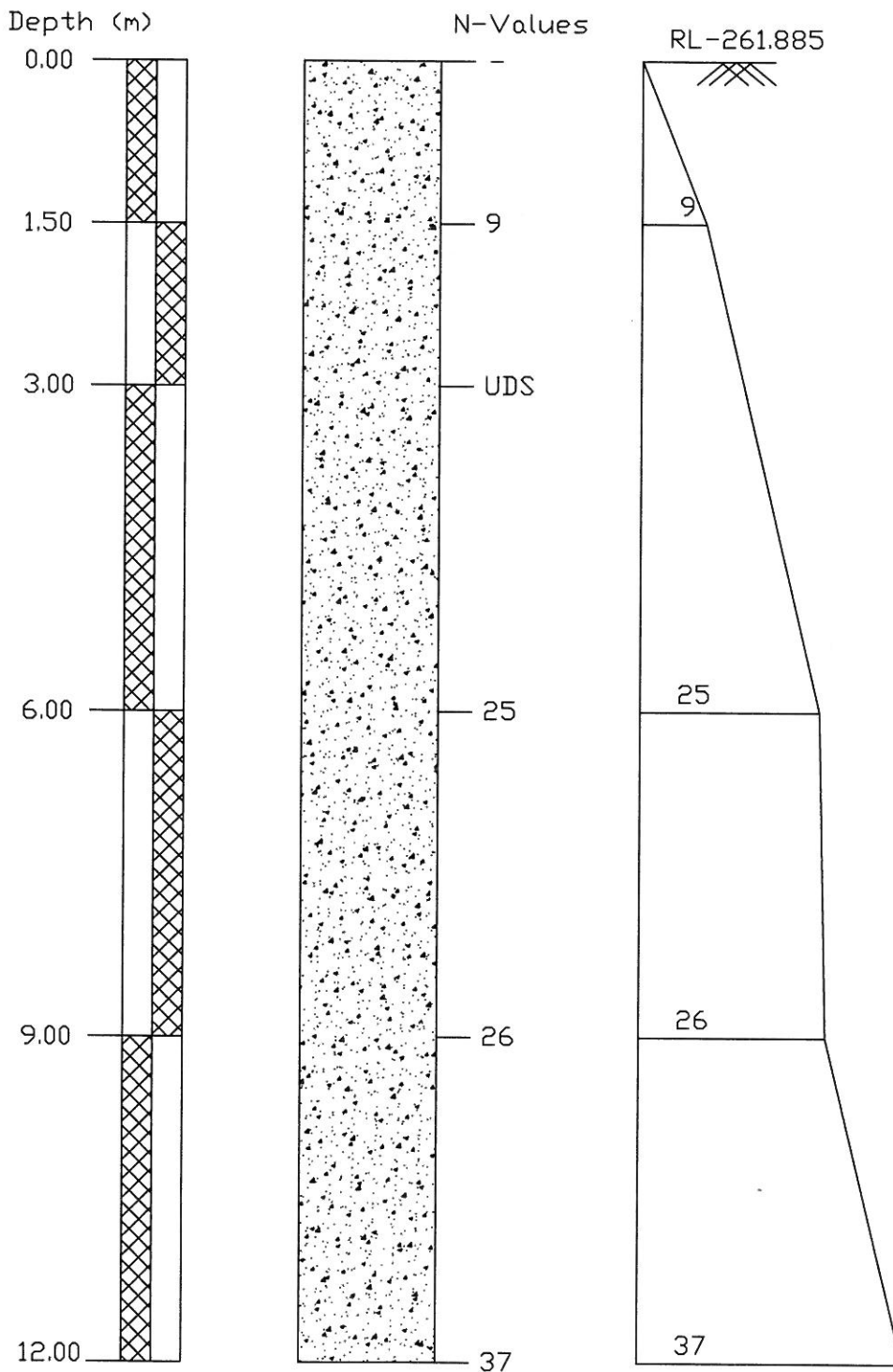


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DFCCIL KESARI TO SAMEHWAL

3297

BORELOG OF BH-1(LHS) AT EXISTING KM-346/1 FOR ALIGNMENT
ON KESARI TO SANEHWAL, LUDHIANA



3298

LEGEND

SYMBOL	DESCRIPTION
	SILTY SAND

ANNEXURE - III

Calculation of SBC for shallow foundations as per IS : 6403 - 1981

INPUT DATA

	Alignment at Ch 346/1	BH-1
<i>Type of footing</i>		
1 Continuous Strip		
2 Rectangular	Rectangular	2
3 Square		
4 Circular		

Angle of internal friction (ϕ°)	26.00
Cohesion (c in t/m ²)	0.00
Void ratio (e)	0.69
Direction of load with vertical (β°)	0.00
Density of surcharge (t/m ³)	1.69
Density of foundation soil (t/m ³)	1.69
Depth of water table(m)	1.50
Factor of safety	3.00

S.no.	Depth (m)	Width (m)	Length (m)
1	1.50	3.00	8.00
2	3.00	3.00	8.00
3	4.50	3.00	8.00
4	6.00	3.00	8.00

SHEAR FAILURE CRITERIA

Assumptions and formula used in calculation as per IS:6403-1981 are given below -

The ultimate net bearing capacity in case of general shear failure is given by

$$q_d = c N_c s_c d_c i_c + q (N_q - 1) s_q d_q i_q + (1/2) B \gamma N_\gamma s_\gamma d_\gamma i_\gamma W'$$

The ultimate net bearing capacity in case of local shear failure is given by

$$q'_d = (2/3) c N'_c s_c d_c i_c + q (N'_q - 1) s_q d_q i_q + (1/2) B \gamma N'_\gamma s_\gamma d_\gamma i_\gamma W'$$

Where,

$$d_c = 1 + 0.2 (D_f/B) * \text{SQRT}(N_b)$$

$$d_q = d_\gamma = 1 \text{ for } \phi < 10^\circ$$

$$d_q = d_\gamma = 1 + 0.1 (D_f/B) * \text{SQRT}(N_b) \text{ for } \phi > 10^\circ$$

$$N_b = \tan^2(\pi/4 + \phi/2)$$

$$\phi' \text{ for local shear failure} = \tan^{-1} (0.67 \tan \phi)$$

OUTPUT

The computer aided results for shear failure criteria are tabulated below. The results are interpolated values of bearing capacity obtained from general and local shear failure criteria.

3299

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ANNEXURE - III

Bearing capacity factors :

ϕ	26.00
N_c	22.60
N_q	12.21
N_γ	13.18

ϕ'	18.10
N'_c	13.36
N'_q	5.46
N'_γ	4.35

Shape factors :

S.no.	Width(m)	Length (m)	S_c	S_q	S_γ
1	3.00	8.00	1.08	1.08	0.85
2	3.00	8.00	1.08	1.08	0.85
3	3.00	8.00	1.08	1.08	0.85
4	3.00	8.00	1.08	1.08	0.85

Depth factors :

S.no.	Depth(m)	Width(m)	d_c	d_q	d_γ
1	1.50	3.00	1.16	1.08	1.08
2	3.00	3.00	1.32	1.16	1.16
3	4.50	3.00	1.48	1.24	1.24
4	6.00	3.00	1.64	1.32	1.32

Inclination factors :

$i_c = (1 - \alpha / 90)^2$	$i_q = (1 - \alpha / 90)^2$	$i_\gamma = (1 - \alpha / \phi)^2$
1.00	1.00	1.00

Water table factor :

S.no.	Depth(m)	Width(m)	Z_w/B	W'
1	1.50	3.00	0.00	0.50
2	3.00	3.00	-0.50	0.50
3	4.50	3.00	-1.00	0.50
4	6.00	3.00	-1.50	0.50

Safe Bearing Capacity

S.no.	Depth(m)	Width(m)	Length (m)	SBC in (t/m^2)		
				General shea	Local shear	Actual
1	1.50	3.00	8.00	16.11	6.06	9.08
2	3.00	3.00	8.00	29.11	11.22	16.59
3	4.50	3.00	8.00	31.12	11.99	17.73
4	6.00	3.00	8.00	33.13	12.77	18.87

3300

ANNEXURE - IV

Settlement Calculation As per IS 8009 (Part 1)			
Location	Alignment		
Chainage	346/1		
Bore Hole No.	1		
Footing Depth (m)	1.50	Footing Depth (m)	3.00
SBC (t/m ²)	9.00	SBC (t/m ²)	16.00
Average N value	17	Average N value	21
Settlement for 10 t/m ² (mm)	18.00	Settlement for 10 t/m ² (mm)	15.00
Settlement (mm) for SBC	16.20	Settlement (mm) for SBC	24.00
Depth Correction	0.91	Depth Correction	0.83
Rigidity Correction	0.8	Rigidity Correction	0.8
Corrected Total Settlement (mm)	11.8	Corrected Total Settlement (mm)	15.9

Footing Depth (m)	4.50
SBC (t/m ²)	17.50
Average N value	21
Settlement for 10 t/m ² (mm)	14.40
Settlement (mm) for SBC	25.20
Depth Correction	0.74
Rigidity Correction	0.8
Corrected Total Settlement (mm)	14.9

Footing Depth (m)	6.00
SBC (t/m ²)	19.00
Average N value	22
Settlement for 10 t/m ² (mm)	14.00
Settlement (mm) for SBC	26.60
Depth Correction	0.68
Rigidity Correction	0.8
Corrected Total Settlement (mm)	14.5

3301

306

CHAPTER - 35

"Alignment"

Location - Existing Km. - 344/1

3302

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35.1 LOCATION OF STRUCTURE:

Alignment at existing km 344/1.

35.2 BOREHOLE DESCRIPTIONS:

- Location of Structure, Boreholes with RL shown in **FIGURE-1**.
- Subsurface Characteristic of Soil/Rock shown in **ANNEXURE-I**.
- Borelogs and sub soil profile shown in **ANNEXURE-II**.
- Calculations of Safe Bearing Capacities in **ANNEXURE-III**.
- Calculations of Probable Settlement in **ANNEXURE-IV**.
- Depth of water Table $\geq 30.00\text{m}$ below EGL.

Subsurface profile at the site

BOREHOLE No.	Depth (m)	Type of Soil/Rock	Soil/Rock Characteristics
BH-1	0.00 to 3.00	Silty Sand	Loose
	3.00 to 9.00	Silty Sand	Medium Dense
	9.00 to 12.00	Silty Sand	Dense
	Below 12.00	Sandy Silt with Clay	Dense

35.3 CHEMICAL ANALYSIS OF SOIL:

BOREHOLE		CHEMICAL PROPERTIES					
No.	Depth (m)	pH	Carbonate %	Chlorides %	Sulphate %	Nitrate %	Salinity %
BH-1	3.00	8.50	0.009	0.0018	NIL	0.0010	0.021

35.4 DIFFERENTIAL FREE SWELL INDEX (DFS)

Bore Hole No.	Depth (m)	DFS Index in %
BH-1	6.00	NIL

35.6 NET ALLOWABLE BEARING PRESSURE

Borehole No.	Depth from EGL (m)	Net Allowable Bearing Pressure (t/m ²)
BH-1	1.50	13.00
	3.00	17.50
	4.50	27.00
	6.00	33.00

35.7 CONCLUSIONS

- Subsurface Profiles indicates suitable Soil formation for foundations.

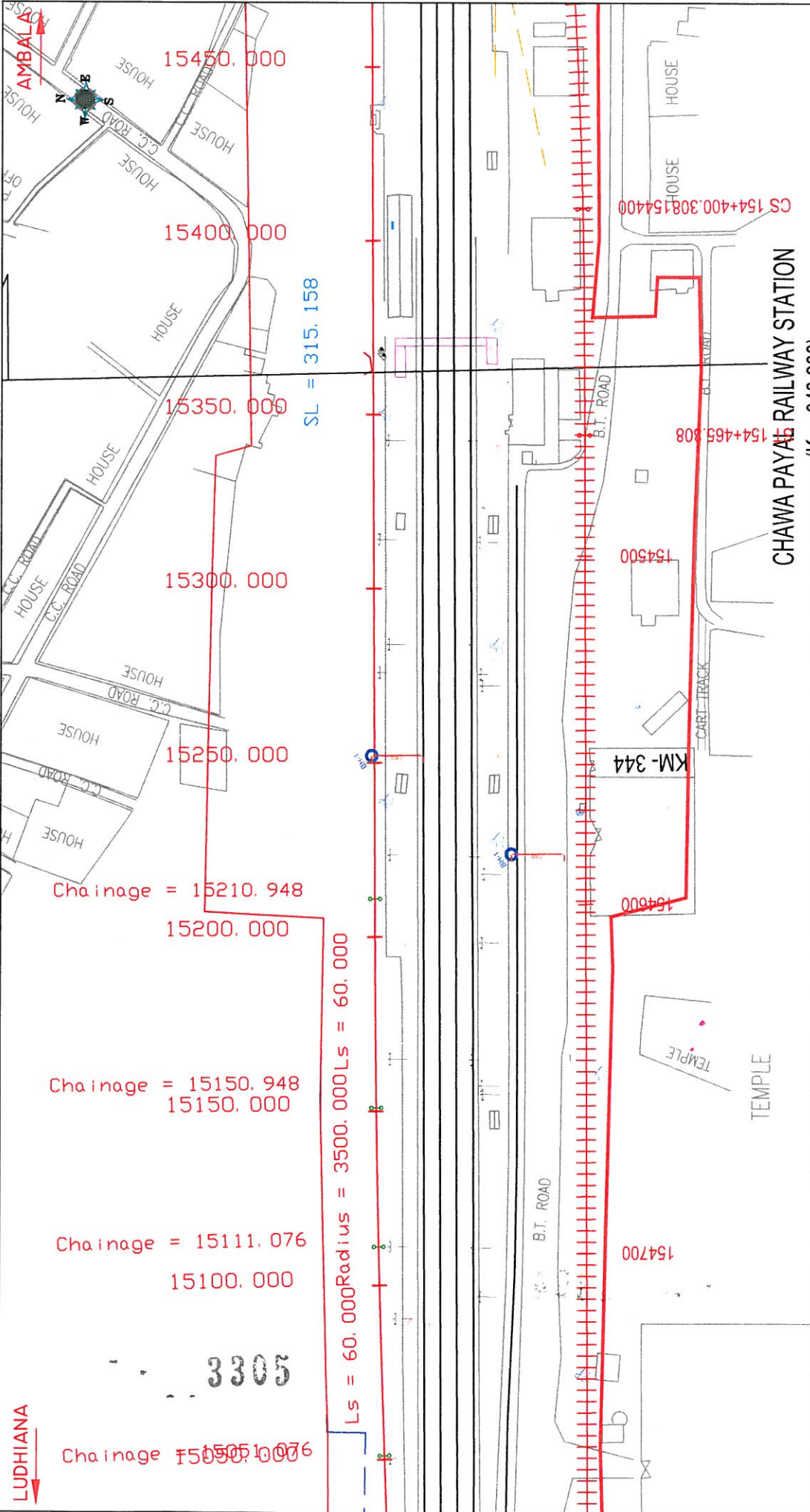
3303

35.8 RECOMMENDATIONS

(i)	<i>Type of foundation</i>	Open foundation
(ii)	<i>Depth of foundation below GL</i>	Below 2.00 m from EGL

Note- The above recommendations are based on the field and laboratory tests conducted on the soil, and our experience in this regard. If the actual subsoil conditions during excavation for the foundation differ from the observations reported here, the design experts/consultants should be referred for suggestion, further investigations. However, the Depth and Type of foundation is to be decided by the structure designer depending upon the type of loading/structure and site conditions.

3304



<p>ALL DIMENSIONS IN METER</p>	<p>PROJECT :-</p>	<p>DESIGN :-</p>
<p>FIG. :-1 LOCATION PLAN OF PROPOSED ALIGNMENT AT CH. 344/1</p>	<p>RL OF BH-I = 262.602</p>	<p>LUDHIANA-AMBALA (DFCCIL)</p>
<p>CONSULTING ENGINEERS GROUP LTD. E-12, Meji Colony, Malviya Nagar, Jaipur-17 Tel: 91-141-2520899, 2521899, 2520556 Fax: 2521346, E-Mail: ce@cegroupindia.com</p>		

ANNEXURE - I

Geotechnical Report

SOIL CHARACTERISTICS OF BORE HOLE AT BH-1 (LHS) OF ALIGNMENT AT CHAINAGE 344/1																			
Project :	Chainage 344/1		Date of Testing	Location at	B.H. No.	Depth of Water Table	Termination Depth		Surface Elevation		Ref. Code								
	Observed	Correction					Corrected	1	1 (LHS)	below 30.00 m.	12.00mtr	262.602	Specific Gravity	Shear Strength					
Depth from GL (m)	N	C _u	N _c	Clay	Silt	Grain Size Distribution % wt retained			B.D.	M.C.	D.D.	c	φ						
						Fine	Medium	Coarse	Fine	Coarse	L.L.	P.L.	P.I.	gm/cc	%	gm/cc	kg/cm ²	degree	
0.00	-	-	-	3.18	5.95	79.61	9.35	1.23	0.68	0.00	26	NIL	NP	-	-	-	-	-	-
1.50	9	1.45	13.05	3.10	8.02	84.48	3.49	0.00	0.91	0.00	27	NIL	NP	-	-	-	-	-	-
3.00	11	1.22	13.42	1.82	5.16	84.86	7.90	0.26	0.00	0.00	26	NIL	NP	-	-	-	-	-	-
6.00	UDS	-	-	2.97	6.73	77.91	10.39	2.00	0.00	0.00	25	NIL	NP	1.74	5.59	1.65	0.00	27.50	-
9.00	44	0.85	37.40	2.15	8.67	82.64	6.23	0.31	0.00	0.00	25	NIL	NP	-	-	-	-	-	-
12.00	46	0.76	34.96	12.67	73.50	10.42	0.58	0.95	1.88	0.00	27	18	9	-	-	-	-	-	-

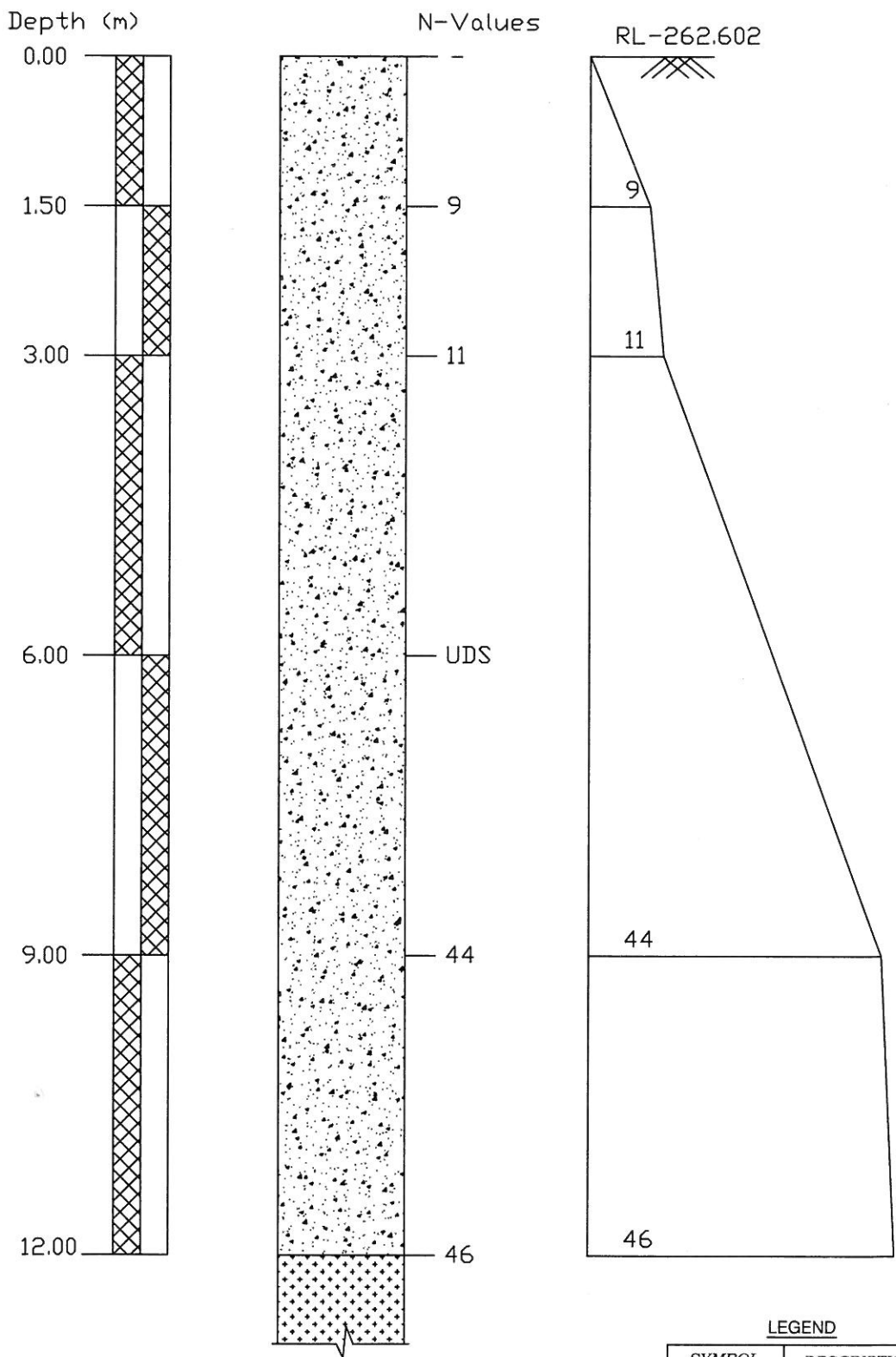


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DFCCIL KESARI TO SANEHWAL

3306

BORELOG OF BH-1(LHS) AT EXISTING KM-344/1 FOR ALIGNMENT
ON KESARI TO SANEHWAL, LUDHIANA



3307

LEGEND

SYMBOL	DESCRIPTION
	SILTY SAND
	SANDY SILT WITH CLAY

ANNEXURE - III

Calculation of SBC for shallow foundations as per IS : 6403 - 1981

INPUT DATA

	Alignment at Ch 344/1	BH-1
<i>Type of footing</i>		2
1 Continuous Strip		
2 Rectangular	<i>Rectangular</i>	
3 Square		
4 Circular		
Angle of internal friction (ϕ°)		27.50
Cohesion (c in t/m ²)		0.00
Void ratio (e)		0.61
Direction of load with vertical (ρ°)		0.00
Density of surcharge (t/m^3)		1.70
Density of foundation soil (t/m^3)		1.74
Depth of water table(m)		1.50
Factor of safety		3.00

S.no.	Depth (m)	Width (m)	Length (m)
1	1.50	3.00	8.00
2	3.00	3.00	8.00
3	4.50	3.00	8.00
4	6.00	3.00	8.00

SHEAR FAILURE CRITERIA

Assumptions and formula used in calculation as per IS:6403-1981 are given below -

The ultimate net bearing capacity in case of general shear failure is given by

$$q_d = c N_c s_c d_c i_c + q (N_q - 1) s_q d_q i_q + (1/2) B \gamma N_\gamma s_\gamma d_\gamma i_\gamma W$$

The ultimate net bearing capacity in case of local shear failure is given by

$$q'_d = (2/3) c N'_c s_c d_c i_c + q (N'_q - 1) s_q d_q i_q + (1/2) B \gamma N'_\gamma s_\gamma d_\gamma i_\gamma W$$

Where,

$$d_c = 1 + 0.2 (D_f/B) * \text{SQRT}(N_b)$$

$$d_q = d_\gamma = 1 \text{ for } \phi < 10^\circ$$

$$d_q = d_\gamma = 1 + 0.1 (D_f/B) * \text{SQRT}(N_b) \text{ for } \phi > 10^\circ$$

$$N_b = \tan^2(\pi/4 + \phi/2)$$

$$\phi' \text{ for local shear failure} = \tan^{-1} (0.67 \tan \phi)$$

OUTPUT

The computer aided results for shear failure criteria are tabulated below. The results are interpolated values of bearing capacity obtained from general and local shear failure criteria.

3308



ANNEXURE - III

Bearing capacity factors :

ϕ	27.50
N_c	25.43
N_q	14.53
N_γ	16.64

ϕ'	19.23
N'_c	14.24
N'_q	6.02
N'_γ	4.97

Shape factors :

S.no.	Width(m)	Length (m)	S_c	S_q	S_γ
1	3.00	8.00	1.08	1.08	0.85
2	3.00	8.00	1.08	1.08	0.85
3	3.00	8.00	1.08	1.08	0.85
4	3.00	8.00	1.08	1.08	0.85

Depth factors :

S.no.	Depth(m)	Width(m)	d_c	d_q	d_γ
1	1.50	3.00	1.16	1.08	1.08
2	3.00	3.00	1.33	1.16	1.16
3	4.50	3.00	1.49	1.25	1.25
4	6.00	3.00	1.66	1.33	1.33

Inclination factors :

$i_c = (1 - \alpha / 90)^2$	$i_q = (1 - \alpha / 90)^2$	$i_\gamma = (1 - \alpha / \phi)^2$
1.00	1.00	1.00

Water table factor :

S.no.	Depth(m)	Width(m)	Z_w/B	W'
1	1.50	3.00	0.00	0.50
2	3.00	3.00	-0.50	0.50
3	4.50	3.00	-1.00	0.50
4	6.00	3.00	-1.50	0.50

Safe Bearing Capacity

S.no.	Depth(m)	Width(m)	Length (m)	SBC in (t/m^2)		
				General shea	Local shear	Actual
1	1.50	3.00	8.00	20.04	6.95	16.11
2	3.00	3.00	8.00	35.97	12.83	29.02
3	4.50	3.00	8.00	38.51	13.73	31.08
4	6.00	3.00	8.00	41.06	14.64	33.13

3309

ANNEXURE - IV

Settlement Calculation As per IS 8009 (Part 1)	
Location	Alignment
Chainage	344/1
Bore Hole No.	1

Footing Depth (m)	1.50
SBC (t/m ²)	13.00
Average N value	15
Settlement for 10 t/m ² (mm)	21.00
Settlement (mm) for SBC	27.30
Depth Correction	0.91
Rigidity Correction	0.8
Corrected Total Settlement (mm)	19.9

Footing Depth (m)	3.00
SBC (t/m ²)	17.50
Average N value	15
Settlement for 10 t/m ² (mm)	21.00
Settlement (mm) for SBC	36.75
Depth Correction	0.83
Rigidity Correction	0.8
Corrected Total Settlement (mm)	24.4

Footing Depth (m)	4.50
SBC (t/m ²)	27.00
Average N value	19
Settlement for 10 t/m ² (mm)	15.00
Settlement (mm) for SBC	40.50
Depth Correction	0.74
Rigidity Correction	0.8
Corrected Total Settlement (mm)	24.0

Footing Depth (m)	6.00
SBC (t/m ²)	33.00
Average N value	25
Settlement for 10 t/m ² (mm)	12.00
Settlement (mm) for SBC	39.60
Depth Correction	0.68
Rigidity Correction	0.8
Corrected Total Settlement (mm)	21.5

3310

CHAPTER - 36

"Alignment",

Location - Existing Km. - 343/1

3311



36.1 LOCATION OF STRUCTURE:

Alignment at existing km 343/1.

36.2 BOREHOLE DESCRIPTIONS:

- Location of Structure, Boreholes with RL shown in **FIGURE-1**.
- Subsurface Characteristic of Soil/Rock shown in **ANNEXURE-I**.
- Borelogs and sub soil profile shown in **ANNEXURE-II**.
- Calculations of Safe Bearing Capacities in **ANNEXURE-III**.
- Calculations of Probable Settlement in **ANNEXURE-IV**.
- Depth of water Table $\geq 30.00\text{m}$ below EGL.

Subsurface profile at the site

BOREHOLE No.	Depth (m)	Type of Soil/Rock	Soil/Rock Characteristics
BH-1	0.00 to 1.50	Sandy Silt with Clay	Loose
	1.50 to 3.00	Sandy Silt with Clay & Gravels	Medium Dense
	3.00 to 6.00	Silty Sand with Gravels	Medium Dense
	6.00 to 12.00	Sandy Silt with Gravels	Medium Dense

36.3 CHEMICAL ANALYSIS OF SOIL:

BOREHOLE		CHEMICAL PROPERTIES					
No.	Depth (m)	pH	Carbonate %	Chlorides %	Sulphate %	Nitrate %	Salinity %
BH-1	3.00	8.70	0.003	0.0019	NIL	0.0012	0.013

36.4 DIFFERENTIAL FREE SWELL INDEX (DFS)

Bore Hole No.	Depth (m)	DFS Index in %
BH-1	3.00	NIL
	9.00	NIL

36.5 NET ALLOWABLE BEARING PRESSURE

Borehole No.	Depth from EGL (m)	Net Allowable Bearing Pressure (t/m^2)
BH-1	1.50	12.50
	3.00	17.00
	4.50	18.50
	6.00	20.00

36.6 CONCLUSIONS

- Subsurface Profiles indicates suitable Soil formation for foundations.

36.7 RECOMMENDATIONS

(i)	<i>Type of foundation</i>	Open foundation
(ii)	<i>Depth of foundation below GL</i>	Below 2.00m from EGL

Note- The above recommendations are based on the field and laboratory tests conducted on the soil, and our experience in this regard. If the actual subsoil conditions during excavation for the foundation differ from the observations reported here, the design experts/consultants should be referred for suggestion, further investigations. However, the Depth and Type of foundation is to be decided by the structure designer depending upon the type of loading/structure and site conditions.

3318

LUDHIANA

AMBALA

AG. LAND



16100.000

16150.000

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16250.000

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16400.000

3314

BH-1

1100

B.T. ROAD

153700

153600

KM-343

153500

153400

ALL DIMENSIONS IN METER

PROJECT :-

DESIGN :-

FIG. :-1
LOCATION PLAN OF PROPOSED ALIGNMENT
AT CH. 343/1

RL OF BH-1 = 260.094

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ANNEXURE - I

SOIL CHARACTERISTICS OF BORE HOLE AT BH-1 (LHS) OF ALIGNMENT AT CHAINAGE 343/1

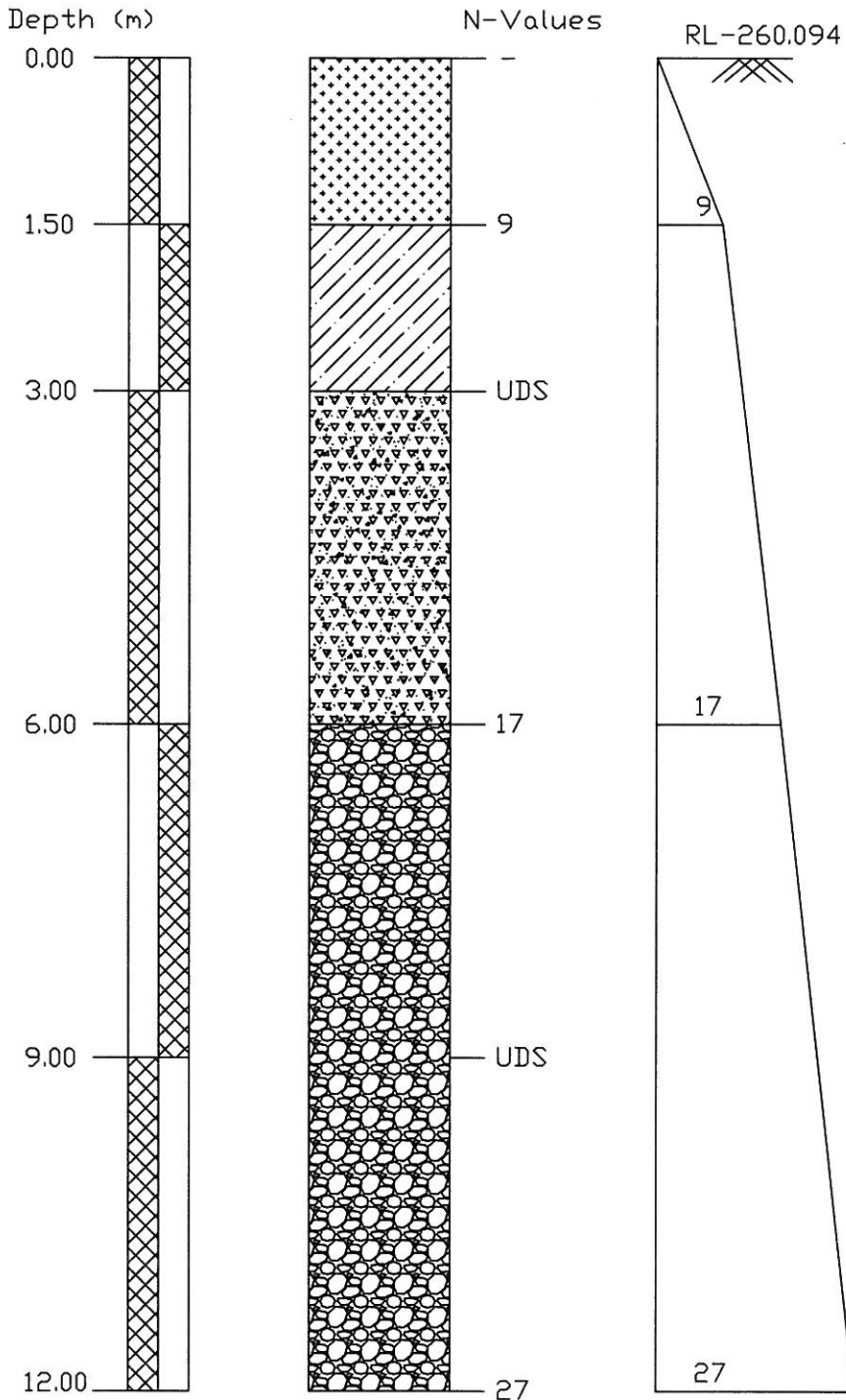
Project :	Chainage 343/1			Date of Testing		Location at	B.H. No.	Depth of Water Table	Termination Depth			Surface Elevation			Ref. Code							
	Observed	Correction Factor	Corrected	31.05.2009 to 31.05.2009	Clay				Silt	Grain Size Distribution % wt retained	Atterberg Limits %	P.L.	P.I.	B.D.	M.C.	D.D.	Specific Gravity	Shear Strength				
Depth from GL (m)	N	C _n	N _n	Soil Description (Soil Group)	Clay	Silt	Fine	Medium	Coarse	Fine	Coarse	L.L.	P.L.	P.I.	gm/cc	%	gm/cc	D.D.	Specific Gravity	c kg/cm ²	φ degree	
0.00	-	-	-	Sandy Silt with Clay	10.63	64.44	12.39	6.39	4.16	1.38	0.61	27	19	8	-	-	-	-	-	-	-	-
1.50	9	1.45	13.05	Sandy Silt with Clay & Gravels	8.62	50.98	14.58	2.21	5.66	17.95	0.00	26	18	8	-	-	-	-	-	-	-	-
3.00	UDS	-	-	Silty Sand with Gravels	1.95	12.55	48.20	1.69	1.25	26.25	8.11	24	NIL	NP	1.75	5.30	1.66	2.64	0.00	27.00	-	-
6.00	17	0.99	16.83	Sandy Silt with Gravels	2.26	69.55	8.52	4.11	3.37	12.19	0.00	28	NIL	NP	-	-	-	-	-	-	-	-
9.00	UDS	-	-	Sandy Silt with Gravels	3.20	72.02	12.62	3.26	1.62	6.34	0.94	26	NIL	NP	1.79	6.21	1.68	2.66	0.00	28.00	-	-
12.00	27	0.75	20.25	Sandy Silt with Gravels	1.65	70.87	10.97	4.26	3.21	7.94	1.10	24	NIL	NP	-	-	-	-	-	-	-	-



COMSULTING
Engineers Group Ltd.

DFCCIL KESARI TO SAMEHWAL

BORELOG OF BH-1(LHS) AT EXISTING KM-343/1 FOR ALIGNMENT
ON KESARI TO SANEHWAL, LUDHIANA



LEGEND

SYMBOL	DESCRIPTION
	SANDY SILT WITH CLAY
	SANDY SILT WITH CLAY & GRAVELS
	SILTY SAND WITH GRAVELS
	SANDY SILT WITH GRAVELS

3316

ANNEXURE - III

Calculation of SBC for shallow foundations as per IS : 6403 - 1981

INPUT DATA

	Alignment at Ch 343/1	BH-1
<i>Type of footing</i>		2
1 Continuous Strip		
2 Rectangular	Rectangular	
3 Square		
4 Circular		
Angle of internal friction (ϕ°)		27.00
Coesion (c in t/m ²)		0.00
Void ratio (e)		0.59
Direction of load with vertical (β°)		0.00
Density of surcharge (t/m^3)		1.70
Density of foundation soil (t/m^3)		1.75
Depth of water table(m)		1.50
Factor of safety		3.00

S.no.	Depth (m)	Width (m)	Length (m)
1	1.50	3.00	8.00
2	3.00	3.00	8.00
3	4.50	3.00	8.00
4	6.00	3.00	8.00

SHEAR FAILURE CRITERIA

Assumptions and formula used in calculation as per IS:6403-1981 are given below -

The ultimate net bearing capacity in case of general shear failure is given by

$$q_d = c N_c s_c d_c i_c + q (N_q - 1) s_q d_q i_q + (1/2) B \gamma N_\gamma s_\gamma d_\gamma i_\gamma W'$$

The ultimate net bearing capacity in case of local shear failure is given by

$$q'_d = (2/3) c N'_c s'_c d'_c i'_c + q (N'_q - 1) s'_q d'_q i'_q + (1/2) B \gamma N'_\gamma s'_\gamma d'_\gamma i'_\gamma W'$$

Where,

$$d_c = 1 + 0.2 (D_f/B) * \text{SQRT}(N_\phi)$$

$$d_q = d_\gamma = 1 \text{ for } \phi < 10^\circ$$

$$d_q = d_\gamma = 1 + 0.1 (D_f/B) * \text{SQRT}(N_\phi) \text{ for } \phi > 10^\circ$$

$$N_\phi = \tan^2(\pi/4 + \phi/2)$$

$$\phi' \text{ for local shear failure} = \tan^{-1} (0.67 \tan \phi)$$

OUTPUT

The computer aided results for shear failure criteria are tabulated below. The results are interpolated values of bearing capacity obtained from general and local shear failure criteria.

3317



ANNEXURE - III

Bearing capacity factors :

ϕ	27.00
N_c	24.49
N_q	13.76
N_γ	15.49

ϕ'	18.85
N'_c	13.94
N'_q	5.83
N'_γ	4.76

Shape factors :

S.no.	Width(m)	Length (m)	S_c	S_q	S_γ
1	3.00	8.00	1.08	1.08	0.85
2	3.00	8.00	1.08	1.08	0.85
3	3.00	8.00	1.08	1.08	0.85
4	3.00	8.00	1.08	1.08	0.85

Depth factors :

S.no.	Depth(m)	Width(m)	d_c	d_q	d_γ
1	1.50	3.00	1.16	1.08	1.08
2	3.00	3.00	1.33	1.16	1.16
3	4.50	3.00	1.49	1.24	1.24
4	6.00	3.00	1.65	1.33	1.33

Inclination factors :

$i_c = (1 - \alpha / 90)^2$	$i_q = (1 - \alpha / 90)^2$	$i_\gamma = (1 - \alpha / \phi)^2$
1.00	1.00	1.00

Water table factor :

S.no.	Depth(m)	Width(m)	Z_w/B	W'
1	1.50	3.00	0.00	0.50
2	3.00	3.00	-0.50	0.50
3	4.50	3.00	-1.00	0.50
4	6.00	3.00	-1.50	0.50

Safe Bearing Capacity

S.no.	Depth(m)	Width(m)	Length (m)	SBC in (t/m ²)		
				General shea	Local shear	Actual
1	1.50	3.00	8.00	18.84	6.69	16.41
2	3.00	3.00	8.00	33.82	12.33	29.52
3	4.50	3.00	8.00	36.19	13.20	31.59
4	6.00	3.00	8.00	38.56	14.06	33.66

3318

ANNEXURE - IV

Settlement Calculation As per IS 8009 (Part 1)	
Location	Alignment
Chainage	343/1
Bore Hole No.	1

Footing Depth (m)	1.50
SBC (t/m ²)	12.50
Average N value	14
Settlement for 10 t/m ² (mm)	23.00
Settlement (mm) for SBC	28.75
Depth Correction	0.91
Rigidity Correction	0.8
Corrected Total Settlement (mm)	20.9

Footing Depth (m)	3.00
SBC (t/m ²)	17.00
Average N value	15
Settlement for 10 t/m ² (mm)	21.00
Settlement (mm) for SBC	35.70
Depth Correction	0.83
Rigidity Correction	0.8
Corrected Total Settlement (mm)	23.7

Footing Depth (m)	4.50
SBC (t/m ²)	18.50
Average N value	16
Settlement for 10 t/m ² (mm)	19.00
Settlement (mm) for SBC	35.15
Depth Correction	0.74
Rigidity Correction	0.8
Corrected Total Settlement (mm)	20.8

Footing Depth (m)	6.00
SBC (t/m ²)	20.00
Average N value	17
Settlement for 10 t/m ² (mm)	18.00
Settlement (mm) for SBC	36.00
Depth Correction	0.68
Rigidity Correction	0.8
Corrected Total Settlement (mm)	19.6

3319

CHAPTER - 37

"Alignment",

Location - Existing Km. - 342/1

3320



37.1 LOCATION OF STRUCTURE:

Alignment at existing km 342/1

37.2 BOREHOLE DESCRIPTIONS:

- Location of Structure, Boreholes with RL shown in **FIGURE-1**.
- Subsurface Characteristic of Soil/Rock shown in **ANNEXURE-I**.
- Borelogs and sub soil profile shown in **ANNEXURE-II**.
- Calculations of Safe Bearing Capacities in **ANNEXURE-III**.
- Calculations of Probable Settlement in **ANNEXURE-IV**.
- Depth of water Table $\geq 18.00\text{m}$ below EGL.

Subsurface profile at the site

BOREHOLE No.	Depth (m)	Type of Soil/Rock	Soil/Rock Characteristics
BH-1	0.00 to 1.50	Sandy Silt	Loose
	1.50 to 2.00	Sandy Silt with Clay	Loose
	2.00 to 3.00	Silty Sand	Loose
	3.00 to 12.00	Silty Sand	Medium Dense

37.3 CHEMICAL ANALYSIS OF SOIL:

BOREHOLE		CHEMICAL PROPERTIES					
No.	Depth (m)	pH	Carbonate %	Chlorides %	Sulphate %	Nitrate %	Salinity %
BH-1	3.00	9.10	0.005	0.0012	NIL	0.0011	0.041

37.4 DIFFERENTIAL FREE SWELL INDEX (DFS)

Bore Hole No.	Depth (m)	DFS Index in %
BH-1	3.00	NIL
	9.00	NIL

37.5 NET ALLOWABLE BEARING PRESSURE

Borehole No.	Depth from EGL (m)	Net Allowable Bearing Pressure (t/m ²)
BH-1	1.50	12.00
	3.00	17.50
	4.50	23.00
	6.00	24.00

37.6 CONCLUSIONS

- Subsurface Profiles indicates suitable Soil formation for foundations.

3321

37.7 RECOMMENDATIONS

(i)	<i>Type of foundation</i>	Open foundation
(ii)	<i>Depth of foundation below GL</i>	Below 2.00m from EGL

Note- The above recommendations are based on the field and laboratory tests conducted on the soil, and our experience in this regard. If the actual subsoil conditions during excavation for the foundation differ from the observations reported here, the design experts/consultants should be referred for suggestion, further investigations. However, the Depth and Type of foundation is to be decided by the structure designer depending upon the type of loading/structure and site conditions.

- - 3322

LUDHIANA

AMBALA

AG. LAND



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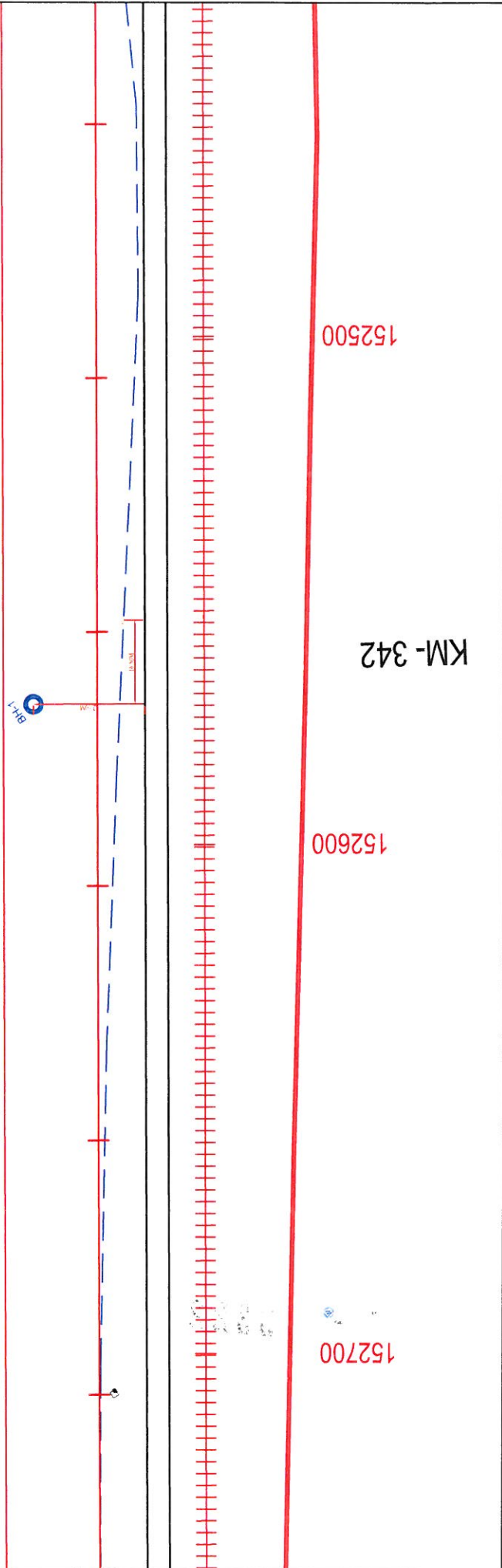
17200.000

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3323



152700

152600

KM-342

152500

ALL DIMENSIONS IN METER

PROJECT :-

FIG :-1
LOCATION PLAN OF PROPOSED ALIGNMENT
AT CH. 342/1

RL OF BH-1 = 260.329

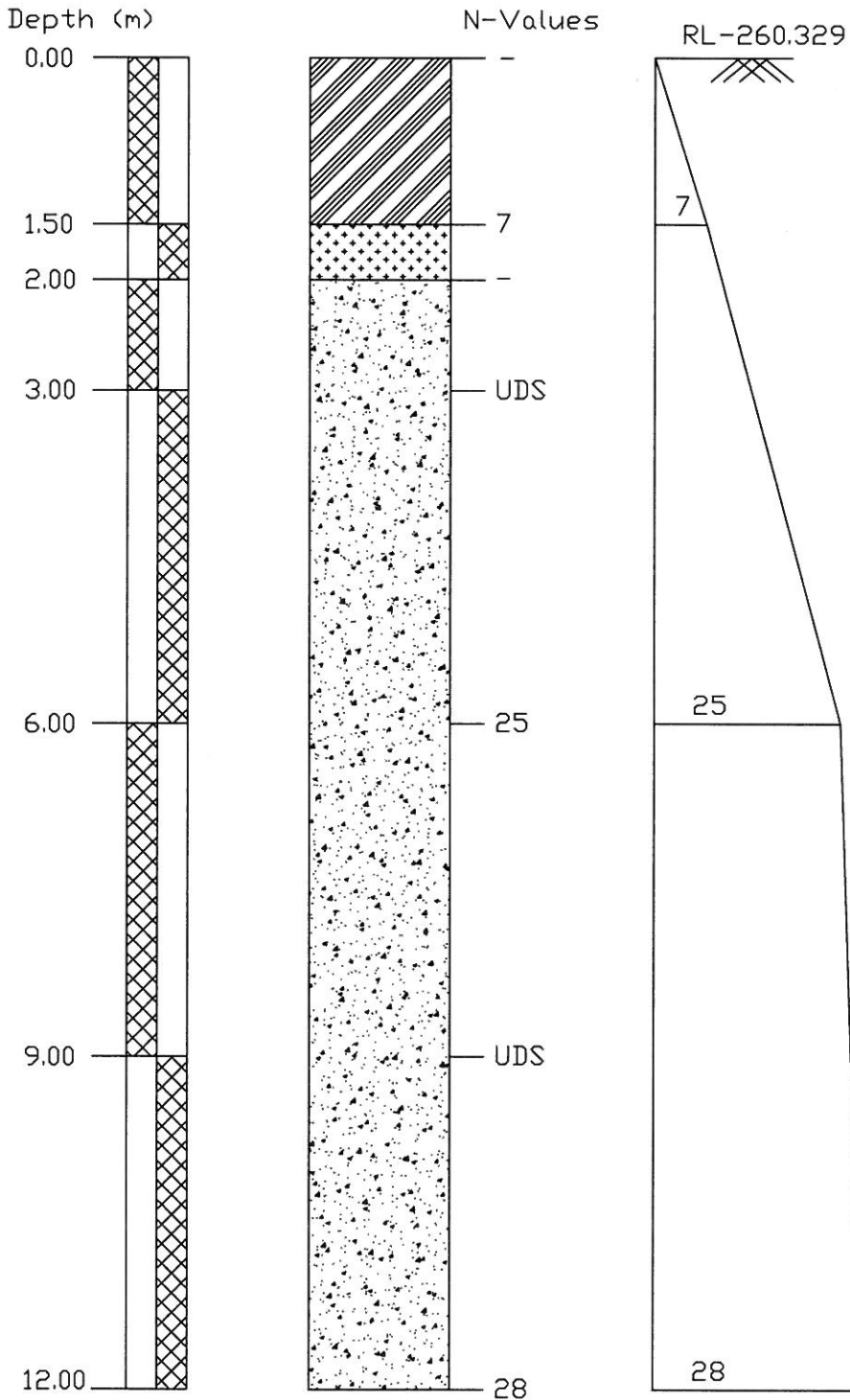
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BORELOG OF BH-1(LHS) AT EXISTING KM-342/1 FOR ALIGNMENT
ON KESARI TO SANEHWAL, LUDHIANA



LEGEND

SYMBOL	DESCRIPTION
	SANDY SILT
	SILTY SAND
	SANDY SILT WITH CLAY

3325

ANNEXURE - III

Calculation of SBC for shallow foundations as per IS : 6403 - 1981

INPUT DATA

	Alignment at Ch 342/1	BH-1
Type of footing		
1 Continuous Strip		
2 Rectangular	Rectangular	2
3 Square		
4 Circular		

Angle of internal friction (ϕ°)	27.50
Cohesion (c in t/m ²)	0.00
Void ratio (e)	0.67
Direction of load with vertical ($^\circ$)	0.00
Density of surcharge (t/m^3)	1.67
Density of foundation soil (t/m^3)	1.67
Depth of water table(m)	1.50
Factor of safety	3.00

S.no.	Depth (m)	Width (m)	Length (m)
1	1.50	3.00	8.00
2	3.00	3.00	8.00
3	4.50	3.00	8.00
4	6.00	3.00	8.00

SHEAR FAILURE CRITERIA

Assumptions and formula used in calculation as per IS:6403-1981 are given below -

The ultimate net bearing capacity in case of general shear failure is given by

$$q_d = c N_c s_c d_c i_c + q (N_q - 1) s_q d_q i_q + (1/2) B \gamma N_\gamma s_\gamma d_\gamma i_\gamma W'$$

The ultimate net bearing capacity in case of local shear failure is given by

$$q'_d = (2/3) c N'_c s_c d_c i_c + q (N'_q - 1) s_q d_q i_q + (1/2) B \gamma N'_\gamma s_\gamma d_\gamma i_\gamma W'$$

Where,

$$d_c = 1 + 0.2 (D_f/B) * \text{SQRT}(N_b)$$

$$d_q = d_\gamma = 1 \text{ for } \phi < 10^\circ$$

$$d_q = d_\gamma = 1 + 0.1 (D_f/B) * \text{SQRT}(N_b) \text{ for } \phi > 10^\circ$$

$$N_b = \tan^2(\pi/4 + \phi/2)$$

$$\phi' \text{ for local shear failure} = \tan^{-1} (0.67 \tan \phi)$$

OUTPUT

The computer aided results for shear failure criteria are tabulated below. The results are interpolated values of bearing capacity obtained from general and local shear failure criteria.

3326



ANNEXURE - III

Bearing capacity factors :

ϕ	27.50
N_c	25.43
N_q	14.53
N_γ	16.64

ϕ'	19.23
N'_c	14.24
N'_q	6.02
N'_γ	4.97

Shape factors :

S.no.	Width(m)	Length (m)	S_c	S_q	S_γ
1	3.00	8.00	1.08	1.08	0.85
2	3.00	8.00	1.08	1.08	0.85
3	3.00	8.00	1.08	1.08	0.85
4	3.00	8.00	1.08	1.08	0.85

Depth factors :

S.no.	Depth(m)	Width(m)	d_c	d_q	d_γ
1	1.50	3.00	1.16	1.08	1.08
2	3.00	3.00	1.33	1.16	1.16
3	4.50	3.00	1.49	1.25	1.25
4	6.00	3.00	1.66	1.33	1.33

Inclination factors :

$i_c = (1 - \alpha / 90)^2$	$i_q = (1 - \alpha / 90)^2$	$i_\gamma = (1 - \alpha / \phi)^2$
1.00	1.00	1.00

Water table factor :

S.no.	Depth(m)	Width(m)	Z_w/B	W
1	1.50	3.00	0.00	0.50
2	3.00	3.00	-0.50	0.50
3	4.50	3.00	-1.00	0.50
4	6.00	3.00	-1.50	0.50

Safe Bearing Capacity

S.no.	Depth(m)	Width(m)	Length (m)	SBC in (t/m ²)		
				General shea	Local shear	Actual
1	1.50	3.00	8.00	19.54	6.79	11.89
2	3.00	3.00	8.00	35.17	12.55	21.60
3	4.50	3.00	8.00	37.66	13.44	23.13
4	6.00	3.00	8.00	40.15	14.33	24.65

3327

ANNEXURE - IV

Settlement Calculation As per IS 8009 (Part 1)	
Location	Alignment
Chainage	342/1
Bore Hole No.	1

Footings Depth (m)	1.50
SBC (t/m ²)	12.00
Average N value	15
Settlement for 10 t/m ² (mm)	21.00
Settlement (mm) for SBC	25.20
Depth Correction	0.91
Rigidity Correction	0.8
Corrected Total Settlement (mm)	18.3

Footings Depth (m)	3.00
SBC (t/m ²)	17.50
Average N value	15
Settlement for 10 t/m ² (mm)	21.00
Settlement (mm) for SBC	36.75
Depth Correction	0.83
Rigidity Correction	0.8
Corrected Total Settlement (mm)	24.4

Footings Depth (m)	4.50
SBC (t/m ²)	23.00
Average N value	22
Settlement for 10 t/m ² (mm)	13.00
Settlement (mm) for SBC	29.90
Depth Correction	0.74
Rigidity Correction	0.8
Corrected Total Settlement (mm)	17.7

Footings Depth (m)	6.00
SBC (t/m ²)	24.00
Average N value	22
Settlement for 10 t/m ² (mm)	13.00
Settlement (mm) for SBC	31.20
Depth Correction	0.68
Rigidity Correction	0.8
Corrected Total Settlement (mm)	17.0

3328

CHAPTER - 38

"Alignment"

Location - Existing Km. - 339/1

3329

ACEG

